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RADC SEISMIC CLASSIFIER DESIGN

Albert H. Proctor, et al

Rome Air Development Center Griffiss Air Force Base, New York

August 1973

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RADC-TR-73-221 Technical Report August 1973



RADC SEISMIC CLASSIFIER DESIGN

Albert H. Proctor James E. Roach Capt. Michael H. Fick

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NATIONAL TECHNICAL INFORMATION SERVICE

Rome Air Development Center Air Force Systems Command Griffiss Air Force Base, New York





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Albert H. Proctor James E. Roach Capt. Michael H. Fick

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#### FOREWORD

This in-house technical report describes work conducted under the Advanced Development Program, Project 692B, Advanced Sensor Technology. The report has been reviewed by Mr. Robert Curtis, Project Engineer, and has been designated as unclassified material.

This report has been reviewed by the Information Office (OI) and is releasable to the National Technical Information Service (NTIS).

This technical report has been reviewed and is approved.

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Chief, Information Sciences Division

FOR THE COMMANDER:

CARLO P. CROCETTI Chief, Plans Office SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

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This report describes the design and evaluation of seismic classifiers for distinguishing humans, heavy trucks, armored personnel carriers, helicopters, and C-131 aircraft. The data used to develop these classifiers consisted of many digitized seismometer responses to each of the intrusion targets and was collected by RADC (DCTI) at the West Lee Test Site. RADC (ISCP) analyzed this waveform data and extracted an initial set of 48 features. The On-Line Pattern Analysis and Recognition System (OLPARS) was then used to

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20. ABSTRACT (continued)

develop several seismic classifier designs which are based on different subsets of the initial 48 features.

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### **ABSTRACT**

This report describes the design and evaluation of seismic classifiers for distinguishing among humans, heavy trucks, armored personnel carriers, helicopters, and C-131 aircraft. The data used to develop these classifiers consisted of many digitized seismometer responses to each of the intrusion targets and was collected by the Sensor Development Section of the Surveillance and Control Division (DCTI) at the West Lee Test Site. The Interactive Processing Section of the Information Sciences Division (ISCP) analyzed this waveform data and extracted an initial set of 48 features. The On-Line Pattern Analysis and Recognition System (OLPARS) was then used to develop several seismic classifier designs which are based on different subsets of the initial 48 features.

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### SECTION I

## INTRODUCTION

This report documents the first attempt to design linear classification logic based on seismic waveform data collected at RADC's West Lee Test Site. This decision logic was designed to distinguish among humans, heavy trucks, armored personnel carriers, helicopters, and C-131 aircraft. The classifier design procedure employed the following sequence of tasks:

- Data Collection
- . Development of an Interactive Graphics Tool for Data Analysis
- . Data Analysis
- . Development of an Automatic Segmentation Algorithm
- . Feature Hypothesis
- . Feature Extraction
- . Feature Evaluation
- . Classification Logic Design
- . Testing Classification Logic with Independent
  Test Data

This effort was conducted in support of Project 692B of the Advanced Sensor Development Program. The seismic classifier designs discussed in this report are based entirely on data collected by the Sensor Development Section at its West Lee Test Site and made available to the Interactive Processing Section for completion of the remaining tasks of the classifier design procedure.

#### SECTION II

## DATA COLLECTION AND CONVERSION

The seismic data base used to design the October 1st
Instrusion Classifier was collected and digitized by PCTI at
the West Lee Test Site in the first quarter of 1972. The
five classes of intrusions observed were helicopters, armored
personnel carriers, C-131 aircraft, heavy trucks, and humans.
Background data was also collected and used to determine a
suitable detection threshold for the turn-on criteria.

The test procedure, following calibration, consisted of running the intruders along one of five specific paths at several known constant speeds. Each intrusion was repeated with each speed, path, and direction as a check on repeatability. Each intrusion involved only one object, with the exception of humans where there were multiple as well as single intrusions. Each sensor was a three-axis low frequency geophone, Geo-Space Model VLF-LP-3D, with one vertical and two horizontal axes (parallel and perpendicular to the intrusion paths).

As the intrusions were taking place, the seismic transducer signals were relayed by underground cables to the site control center, digitized, and recorded directly on digital tapes in the BAMKI format. This format is capable of packing 45 simultaneous sensor waveforms on the tape. Since the experiment involved 3 three-axis geophones, the BAMKI format sparsely packed 9 of 45 possible channels of digitized waveforms on each tape. Each file on the tape contained one intrusion run, consisting of a number of 320 sample records. First, the data was filtered at 500 Hz and then digitized at 1000 samples per second. Each sample value was quantized to any of 1023 values ranging from -2044 to +2044 in steps of 4. The corresponding strip chart range was ± 10 volts maximum. Each test usually produced three or four magnetic tapes. Although the BAMKI format was able to record all the sensor data in real time, it caused many tape read problems which delayed processing the tape at the Honeywell 635.

While the BAMKI format offered some advantages, it also has many deficiencies. The time required to unpack the 45 simultaneous data channels made the BAMKI format unwieldy for quick access and analysis of the data. These tapes contained aborted runs which should have been deleted but were mixed in with the valid runs. Also a software bug in the PDP-9 magnetic tape driver resulted in a high rate of parity errors when we tried to read these tapes at the Honeywell 635. For these reasons, the seismic data was stripped from the BAMKI tapes, edited, and formatted more simply on other tapes. These new tapes presented the advantages of clean, parity error free data and a simple format which made the data easily accessible.

#### SECTION III

### SEGMENTATION

In order to analyze "clean" data, i.e., data which is truly characteristic of each target class, a criterion was developed to cut data from each run and save only a meaningful portion of the run. This segmentation operation is useful because (1) it presents only the statistically significant data to the decision making stage of logic, thus promising higher recognition rates, and (2) it reduces the amount of time the sensor must be processing data for decisions, thus reducing power requirements and extending sensor life.

Development of a segmentation procedure requires one major step in common with feature design: extensive visual study of the waveforms on hardcopy or graphic displays. In a non-trivial problem, valid features can't be selected and designed until the engineers have a very thorough knowledge of the signal characteristics of each class, and optimally a thorough understanding of the physics behind these characteristics. This in-depth knowledge of the data should allow the design of a reasonable segmentation algorithm and criterions. To gain this required information, signal waveforms were recreated and displayed on interactive

graphics devices, such as the CDC 1704 Digigraphics Display and the Tektronics 4002A Graphics Terminal. Estimates of the energy spectrum, using the Fast Fourier Transform, were computed and displayed. Displays and hardcopies of these waveforms and their power spectrums were the tools which enabled the designers to view and analyze the behavior of each class of seismic waveforms.

Since data sementation in the real intrusion detection system will probably be done at the sensor, simplicity and efficiency are of utmost importance. The procedure decided upon begins with calculating the mean value of the entire run, then subtracting that mean from the run (realizable in the field by appropriate capacitive coupling in the sensor's analog output) to eliminate any DC bias. The signal is then full-wave rectified. The average value of each second of the rectified signal is then computed, and a segment of valid data is defined as one for which this one-second average exceeds some threshold  $\theta$  for five consecutive seconds.

Symbolically, given the samples  $\mathbf{f_i}$  of a complete intrusion run, the average absolute value,  $\mathbf{S_k}$ , will be calculated for each consecutive one-second window.

$$S_k = \frac{1}{n} \sum_{i=1}^{n} |f_{nk+i} - \hat{m}|$$
, for the k<sup>th</sup> second

where k = 0, 1, ..., L-1

. L = the number of seconds in the run  $\hat{m} = \frac{1}{N} \sum_{i=1}^{N} f_i = \text{the estimated mean of the run}$ 

n = number of samples per one second window and

N = number of samples in complete run

Segment and save the data in the five second interval if and only if  $S_{\bf k}$  is greater than the threshold  $\theta$  for five consecutive one second windows.

Obvicusly, strong signals, from either large sources or intrusions near to sensors, will result in a greater number of five-second segments. This is desirable, since these stronger signals represent a better signal-to-noise ratio.

The specific segment lengths and thresholds were based on observation and experimentation. The five-second length precluded the acceptance of spurious bursts of noise or brief signal transients as good data. Also, the second-by-second threshold requirement during the five seconds assured that the entire segment was sufficiently strong, instead of having brief but significant lapses into noise. The possibility of triggering this classifier with impulsive noise,

such as explosions, gun-fire, etc. is not likely unless the noise were highly repetitive and sustained over a five second interval.

The threshold, however, required the collection of some statistics. The objective was a threshold which would overlook as much noise as possible, yet which would locate as much valid intrusion data as possible. We selected three representative runs from each data class (including strictly noise runs) and compiled tables of the total time segmented from each run by a variety of thresholds. We then observed, via graphics, the five-second segments selected by thresholds of 20, 30, and 40, and decided that  $\theta = 20$  afforded the best balance between noise rejection and significant data segmentation.

#### SECTION IV

### DATA ANALYSIS

Classifier design requires the analysis of graphic representations of digitized waveforms and their transforms for the purpose of hypothesizing measurements or features which may aid in the discrimination of target classes. This is one of the most important steps in the waveform classification problem because the quality of the selected features directly influences the classifier's performance.

Before data analysis can begin, the researcher must develop or have access to a system which will display his data in some graphic form. At the start of ISCP's involvement in the sensor program, in-house personnel developed a waveform analysis software system on the CDC-1700/Digigraphics System. This waveform analysis tool enabled a user to randomly access and display waveforms or waveform segments and perform operations on the data, such as rectifying, integrating, measuring zero crossings, calculating power spectrums, etc. The major deficiency in this system was its lack of a hard copy capability. Unfortunately, shortly after this interactive graphics software system was operational, the CDC-1700/Digigraphics System was phased out.

Effort was redirected to develop a similar interactive capability on the Honeywell 635, using a remote storage tube terminal as the graphics console. Soon after this development started, it was evident that the development time required for an interactive system in the GECOS III multiprogramming environment was not compatible with the schedule for developing this classifier.

Pattern Analysis and Recognition Corporation (PAR) then made their sensor analysis factility [3] available for this effort.

PAR's sensor analysis facility is designed to analyze acoustic data and is built around a NOVA 800 computer with a 9-track tape unit, card reader, 128K word disk, and a Tektronix 4002A display with hardcopy.

Two software changes had to be made before we could use PAR's facility. First, the BAMKI data stripping program was modified to generate its output on the Honeywell 635's only available nine-track tape drive because the PAR facility's only tape drive was a nine-track unit. Second, PAR modified their system by adding a new input routine to it, which could read the nine-track version of our simplified data format.

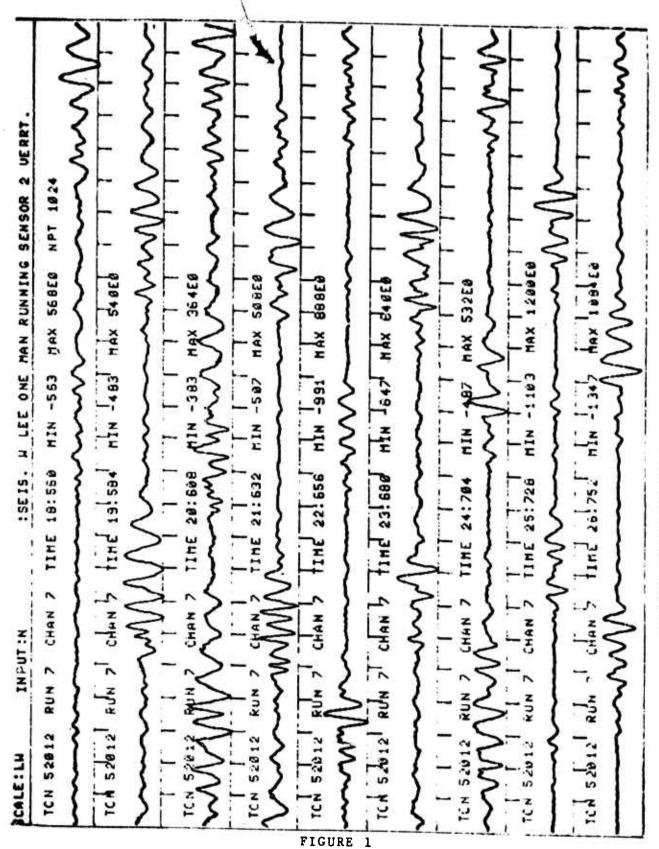
Once we were able to process seismic data from a BAMKI tape, using PAR's facility, a production procedure was set

ur. Three copies of the BAMKI tapes could be left to be processed at night by the 635. Since the Honeywell 635 has only one available nine-track tape drive, only one copy of the BAMKI stripping program was able to execute at a time. Often the BAMKI programs were delayed from executing for long periods of time because the 635's only nine-track tape drive was previously assigned to long batch jobs.

Least one complete run of each intrusion class variation were displayed and hardcopied at the sensor analysis facility. For ground vehicles, these class variations were the different vehicle velocities recorded along each of these paths. For aircraft, these class variations were the different altitudes of the flyovers and the different velocities recorded for each altitude. The class variations for humans were in the number of intruders, path of intrusion, and velocity (feet per second). Examples of time waveform and power spectrum hardcopies for each class are shown in Figures 1 thru 10.

After the hardcopies of the selected intrusion runs were generated, they were added to the hardcopy library. This library consisted of two note books, one containing the time domain waveforms and the other containing power spectrum plots.

A team of ISCP engineers analyzed the data plots contained in the hardcopy library. By comparing the various plots of the intrusion classes looking for within-class similarities and between-class differences, this team compiled a list of 48 potential features. One very useful data plot used in our analysis was the 40-line power spectrum in which each line represents the power spectrums of consecutive one-second windows. The representation of the data in this format enables the analyst to view and compare changes in the power spectrum throughout the duration of the intrusion. Examples of the 40-line power spectrum are shown in Figures 11 and 12. Figure 11 shows the 40-line power spectrum plot of a C-131 aircraft on a radial path over the test site. The frequency shift in the main peaks of the power spectrum indicates when the C-131 responses went through a doppler shift. A similar data display for the UH-1F helicopter, shown in Figure 12, indicates that the doppler shift is not as pronounced for the helicopter as it was for the C-131.



SAMPLE WAVEFORM OF ONE MAN RUNNING

SAMPLE POWER SPECTRUM OF ONE MAN RUNNING

FIGURE 2

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SAMPLE WAVEFORM OF AN ARMOURED PERSONNEL CARRIER

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FIGURE 4

SAMPLE WAVEFORM OF AN M-109 TRUCK

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FIGURE 7

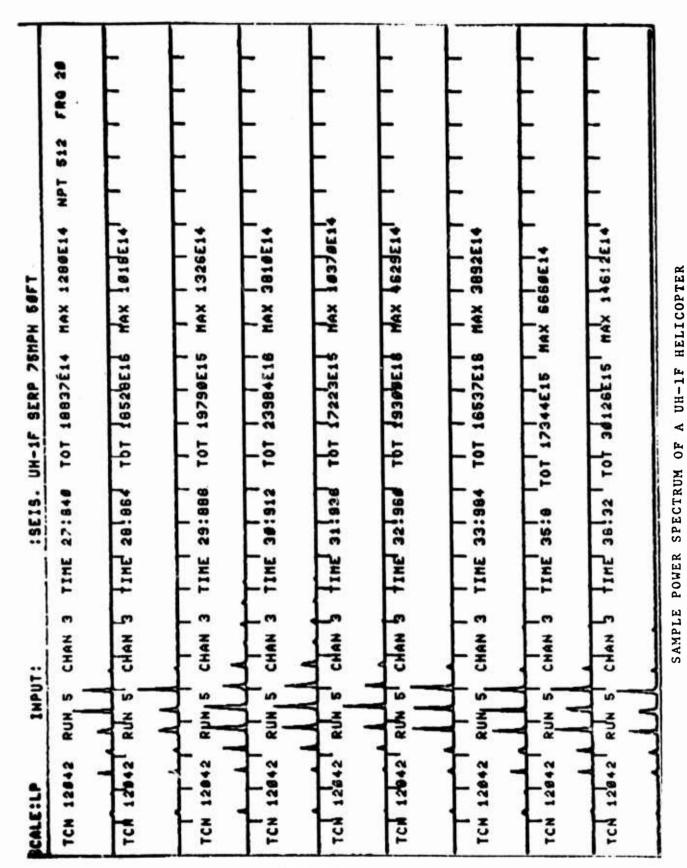


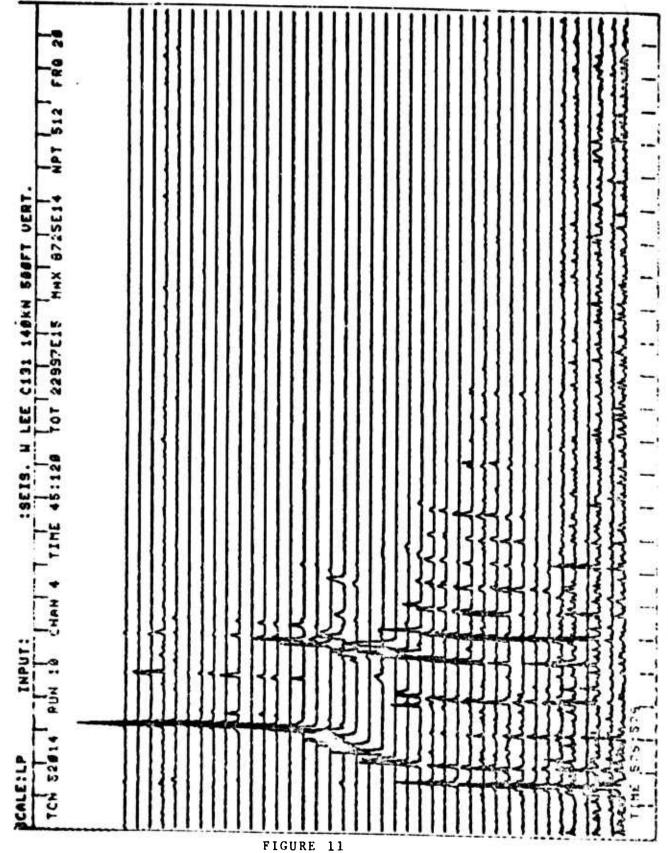
FIGURE 8

FIGURE 9

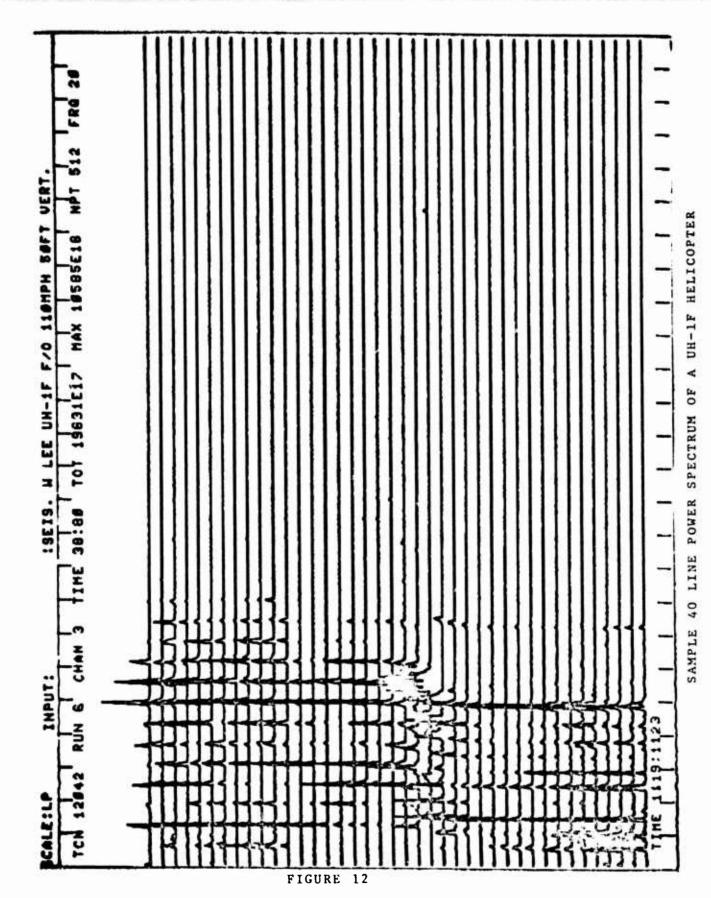
SAMPLE POWER SPECTRUM OF A C-131 AIRCRAFT

FIGURE 21

10



SAMPLE 40 LINE POWER SPECTRUM OF A C-131 AIRCRAFT



#### SECTION V

## FEATURE DEFINITION

Several man-months of studying seismic waveforms on graphics and hardcopy displays produced a set of 24 features for consideration. These features were extracted from one-second (actually 1024 samples, or 1.024 seconds) segments of data and from five-second segments (5120 samples, 5.120 seconds) of data. The two different lengths were selected to evaluate the effect of segment length on classification success. The FFT routine required the number of samples used to be a power of two. Therefore, the one-second window size was chosen to contain 1024 samples instead of 1000. These 24 features taken over the two segment lengths produced a total of 48 features.

The rationale and definitions of the features are given below, in the order in which they appear in the vector data. That is, component 1 of the vector is the average  $\overline{R}$  for one second. Any DDC offset present was subtracted before all processing.

## NO.

## **DEFINITION AND RATIONALE**

1. R for one second (Average R for each halfsecond of a contiguous one-second segment):
R is defined as the ratio of the maximum
absolute signal amplitude during a halfsecond interval to the average absolute

DEFINITION AND RATIONALE (continued)

amplitude for that half second. This
feature appeared a likely candidate for
distinguishing the class of humans, whether
one or several, walking or running. The
impact of a heel gives a sharp, strong
spike in the signal, which decays to noise
level considerably before the next heel
impact. This effect produces a significantly
higher value of R than does a vehicle or
aircraft, since the latter usually produces
high spikes only when the signal is strong
enough to produce a high RMS value.

- 2.  $R^2$  for one second (average  $R^2$  for the two half seconds): Although any information contained in R (e.g., a threshold) will map uniquely into  $R^2$ , squaring R made the distinction between humans and all other classes more obvious to the operator, and eventually to OLPARS.
- $\overline{R}$  for five seconds (average R for 10 contiguous half-second segments).
- 4.  $\mathbb{R}^2$  for 5 seconds.

## NO. DEFINITION AND RATIONALE (continued)

- 5. Harmonic spacing for one second (the most frequently occurring pairwise spacing between the six largest peaks in the power spectrum above 40 Hz): This feature was suggested by the evenly spaced harmonics that were evident in aircraft waveforms.
- 6. Harmonic occurrences in one second (the number of times that the spacing of component 5 above occurred in the one second spectrum): The C-131 usually evidenced harmonics at 20-Hz intervals, the UH-1F helicopter at 12.5 Hz intervals.
- 7. The ratio of the energy between 1 and 20 Hz to that between 21 and 40 Hz for one second (hereafter symbolized by:  $E_{1-20}/E_{21-40}$ ): Although the jeep and APC spectra overlapped considerably, the jeep spectrum did extend somewhat lower than the APC spectrum, which usually dropped off below 20 Hz.
- 8.  $E_{41-60}/E_{21-40}$  for one second: An attempt to separate trucks from APCs.

## NO. DEFINITION AND RATIONALE (continued)

- 9. The number of points in the one second power spectrum which are below 25% of the maximum:

  A coarse amplitude histogram was taken to estimate the value of amplitude information,
- 10. The number of points in the one second power spectrum which are  $\geq 25\%$  and  $\leq 50\%$  of the maximum.
- 11. Number as in 9 and 10 of points  $\geq 50\%$  and <75%.
- 12. Number of spectral points  $\geq 75\%$  of maximum.
- 13. The ratio of the energy above 100 Hz to that below in the one-sec. power spectrum(i.e.  $E_{101-511}/E_{1-100}$ ): Aircraft tend to produce more energy above 100 Hz than do any other classes.
- 14.  $E_{1-5}/E_{1-60}$  for the first second: To estimate the value of spectral distribution information.
- 15.  $E_{6-10}/E_{1-60}$ , first second.
- 16.  $E_{11-15}/E_{1-60}$ , first second.
- 17.  $E_{16-20}/E_{1-60}$ , first second.
- 18.  $E_{21-25}/E_{1-60}$ , first second.
- 19.  $E_{26-30}/E_{1-60}$ , first second.
- 20.

No.	DEFINITION AND RATIONALE (continued)
-----	--------------------------------------

- 25.  $E_{56-60}/E_{1-60}$ , first second.
- 26. The number of peaks in the first one second power spectrum which exceed 10% of the maximum peak.
- 27. Harmonic spacing for the 5-second ensemble average of 5 successive one-second power spectra (see No. 5).
- 28. The number of times the spacing of No. 27 occurs in the 5-second ensemble average (see no. 6).
- 29-48. Components 29-48 are extracted just as components 7-26, in that sequence, except that the spectra observed consist of an ensemble average of 5 consecutive onesecond power spectra instead of a single one-second spectrum.

#### SECTION VI

#### FEATURE EXTRACTION

Once the list of 48 features had been compiled, a batch program was written for the Honeywell 635 to extract these features from the unpacked data tapes. This batch program consists of the main "control" program, a Fast Fourier Transform (FFT) subroutine, a double up algorithm, and a number of feature extraction subroutines.

Data cards direct the control program as to which and how many runs and channels are to be processed. The control program then monitors the specified input data tape channels and calls the feature extraction subroutines when the monitored data channel satisfies the automatic segmentation criteria. The first subroutines called extract features from the time domain waveform segment in the data array X. After these features are extracted, the double up algorithm is called three times to help calculate five consecutive one-second power spectra of the data in X. Since the waveform segments do not have an imaginary component, the double up algorithm enables the FFT to calculate two power spectra with one call to subroutine DOUBLE. After the power spectra are returned, their ensemble average is computed.

The X array will then contain two power spectra of interest, the spectrum for the 1st second and the average spectrum for the five seconds of data. The subroutines which extract features from these two power spectra are then called.

After all the feature extraction subroutines are called, a labeled feature vector is punched out on cards.

After completion of the feature extraction program, the output data deck is taken to the CDC-1604B computer where the feature vectors are transferred to an OLPARS compatible tape.

Listings of the feature extraction program and its subroutines are provided in Appendix  $\Lambda$ .

#### SECTION VII

#### FEATURE EVALUATION

The first step in using the On-Line Pattern Analysis and Recognition System (OLPARS) is to evaluate the discriminatory quality of the extracted features. This enables us to use fewer measurements to achieve a satisfactory classifier design. The OLPARS provides two suboptimal methods for ranking the discriminatory power of the extracted features. Each of these methods provides three types of rankings. The first type uses a significance measure of a particular feature, Xp, for discriminating class i from class j and is designated by  $M_{1,1}(Xp)$ . The second type of ranking uses a significance measure of  $X_p$  for discriminating class i from all other classes and is designated  $M_1(X_p)$ . The last type uses a measure of the overall significance of  $X_p$  for discriminating all classes and is designated  $M(X_p)$ .

The first method in OLPARS for ranking features is the discriminant measure, which is particularly useful when the class conditional probability distributions are unimodal. These discriminant measures, using feature  $X_p$ , are defined as follows:

$$M_{ij}(\chi_p) = \frac{\left[\bar{\chi}_p^{(i)} \quad \bar{\chi}_p^{(j)}\right]^2}{(N_i-1)\left[\hat{\sigma}_p^{(i)}\right]^2 + (N_{j-1})\left[\hat{\sigma}_p^{(j)}\right]^2}$$

$$M_{i}(\chi_{p}) = \sum_{j\neq i}^{\kappa} M_{ij}(\chi_{p})$$

$$M(\chi_p) = \sum_{i=1}^{\kappa} M_i(\chi_p) = \sum_{i=1}^{\kappa} \sum_{j \neq i}^{\kappa} M_{ij}(\chi_p)$$

where  $\overline{\chi}_p^{(j)}$  = the estimated mean of class j along measurement  $\chi_p$ .

 $\hat{\sigma}_{p}^{(j)}$  = the estimated standard deviation of class j along measurement  $\chi_{p}$ .

 $N_{j}$  = the number of samples from class j.

The other OLPARS feature evaluation method is the probability of confusion measure. It is valid for any probability distribution since it essentially measures the overlap of the class conditional probabilities.

Since the functional forms of the class conditional probabilities are not known, OLPARS estimates the marginal class distributions using the sample data. The range for feature  $\chi_p$  is divided into cells of width  $\Delta$ . The probability that a sample from class j will occupy the  $\gamma^{th}$  cell along the range of feature  $\chi_p$  is given by:

$$P_{\gamma p}^{(j)} = \int_{\gamma th} P(\chi_p | c_j) d_{xp}$$

The probability of confusion measures using feature  $\chi_{\mbox{\scriptsize p}}$  are defined as follows:

$$M_{ij}(\chi_p) = 1 - \left[ \sum_{\gamma=1}^{N_p} \min_{\gamma \in \mathcal{I}} \left\{ P_{\gamma p}^{(i)}, P_{\gamma p}^{(j)} \right\} \right]$$

$$M_{i}(\chi_{p}) = \sum_{\substack{j=1\\j\neq i}}^{K} M_{ij}(\chi_{p})$$

$$M(\chi_p) = \sum_{i=1}^K M_i(\chi_p) = \sum_{i=1}^K \sum_{j \neq i}^K M_{i,j}(\chi_p)$$

where  $N_p$  = the number of cells along measurement  $\chi_p$ 

and K = the number of classes.

The ranking of extracted features based on these evaluation techniques provides the information required to rationally choose initial subsets of the 48 features for logic design. Logic design is an iterative process in which many designs, based on modified versions of the initial feature subsets, are generated and tested. Features which appear to discriminate between the more troublesome classes are added, while superfluous features which rank high for

the same easily discriminated classes are eliminated.

For this five-class problem, the top fifteen features, rank-ordered by the probability of confusion measure,  $M_{ij}(\chi_p)$ , are shown in Appendix B.

#### SECTION VIII

#### CLASSIFICATION LOGIC

The classifiers designed by ISCP for this pattern recognition problem consist solely of sets of linear discriminants for ease of hardware implementation. The logic for these classifiers is based on the pairwise Fisher Linear Discriminant Technique. For each pair of classes i and j, a unit vector dij is computed such that projections of the data onto dij maximize the ratio of the between-class scatter to the within-class scatter. The direction dij which maximizes this ratio is given by Reference [5].

$$d_{ij} = \alpha W_{ij}^{-1} \Delta_{ij}$$

where  $W_{ij} = (N_i - 1) C_i + (N_j - 1) C_j$ 

C<sub>ii</sub> = Estimated covariance matrix for class i

∆ij = Li - Lj

 $\mu_i$  = Estimated mean vector of class i

N; = Number of vectors in class i

and  $\alpha$  is a normalizing constant so that  $\left|\frac{d}{dt}\right| = 1$ 

OLPARS computes  $d_{ij}$  and an initial threshold,  $\theta_{ij}$ , to distinguish between all pairs of classes. These thresholds may be adjusted, if necessary, to obtain optimal discrimination along each  $d_{ij}$ .

For example, the inner product of an unknown input feature vector, x, is taken with the discriminant  $\underline{d}_{AH}$  for the pair of APCs and helicopters, compared with the threshold  $\theta_{AH}$  for the pair of APCs and helicopters.

If 
$$\langle \underline{d}_{AH}, \underline{\chi} \rangle = \sum_{i=1}^{\kappa} \chi_i \underline{d}_{AH} > \theta_{AH}$$
 increment the counter for the APC class.

If 
$$\langle \underline{d}_{AH}, \underline{\chi} \rangle = \sum_{i=1}^{\kappa} \chi_i \underline{d}_{AH} \langle \theta_{AH} \rangle$$
 increment the counter for the helicopter class.

If 
$$\langle d_{AH}, \chi \rangle = \sum_{i=1}^{K} \chi_i d_{AH} = \theta_{AH}$$
 increment the counter for the class with the larger number of samples in the design set.

where K = Size of the feature space.

After all the pairwise decisions are made, a binary vote is cast by each comparator and the final decision is determined by the class counter that received the most votes. In case of ties, the decision is given to the class involved in the tie which has the highest a priori probability. The resultant classification scheme is diagrammed in Figure 13.

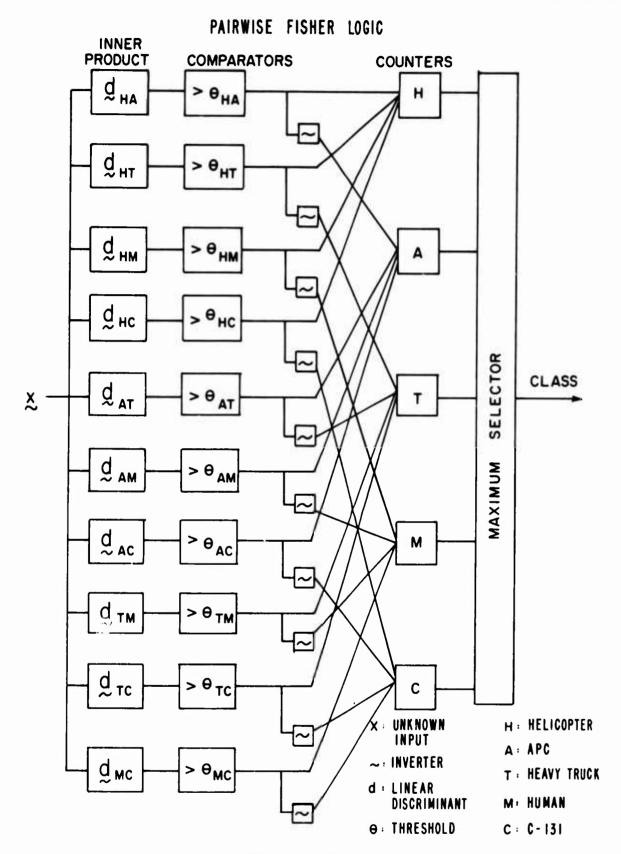


Figure 13.

#### SECTION IX

#### RECOGNITION RATES

Four classifiers were designed using 16, 22, 33, and 44 features. With the exception that feature 46 is missing from the 44 feature design, each design is based on a subset of the features used in the higher order designs. Figure 14 lists the features used for each design.

These classifiers were evaluated with the design data set and an independent test data set. The design set consisted of 715 vectors: 133 vectors from the class of helicopters; 176 for APCs; 135 for heavy trucks; 136 for humans; and 135 represented C-131s. The independent test set was comprised of 607 vectors: 159 for helicopters; 171 for APCs; 16 for heavy trucks; 129 for humans; and 132 for C-131s. The design and test confusion matrices from the resulting evaluation of each classifier are shown in Figures 15 thru 18.

# FEATURE LIST FOR EACH DESIGN

				44 FI	EATURE	DESI	GN		
1	2	3	4	5	6	7	8	9	10
11	13	14	15	16	17	18	19	20	21
22	23	25	26	27	28	29	30	31	32
33	35	36	37	38	39	40	41	42	43
44	45	47	48						
				33 FE	EATURE	DESI	GN		
1	2	3	4	5	6	14	15	16	19
20	21	23	25	27	28	29	30	31	32
33	36	37	38	39	40	41	42	43	44
45	46	47							
				22 FE	ATURE	DESI	GN		
3	4	5	6	14	15	16	25	27	28
29	30	31	37	38	39	42	43	44	45
46	47								
				16 FF	ATURE	DESI	GN		
3	4	27	28	29	30	31	37	38	39
42	43	44	45	46	47				

		ASSI	GNED	CLASS	CLASS		
		Н	Α	Т	M	С	
	Н	125	2	3	2	1	
	Α	0	172	3	1	0	
TRUE CLASS	Т	0	2	133	0	n	
	М	0	1	0	133	2	
	С	0	0	0	1	133	

# CONFUSION MATRIX FOR THE DESIGN SET

### USING 44 FEATURES

14		ASSI	GNED	CLASS	3	
*		Н	٨	Т	R.F.	С
	Н	121	12	3	2	21
	٨	4	137	27	3	0
TRUE CLASS	Т	1	3	12	n	n
	M	0	5	0	123	1
	С	7	1	1	1	122

Probability of Correct Classification = .848

### CONFUSION MATRIX FOR THE TEST SET

# USING 44 FEATURES

LEGEND: H - HELICOPTER M - HUMAN A - APC C - C-131 T - HEAVY TRUCK

		ASSI	IGNED CLASS			
		H	Α	T	M	C
	Н	125	1	4	2	1
TRUE	Ä	4	168	3	1	0
CLASS	Т	0	4	131	0	0
	М	0	1	0	131	4
	С	1	0	0	0	134

# CONFUSION MATRIX FOR THE DESIGN SET

## USING 33 FEATURES

		ASSI	ASSIGNED CLASS			
		Н	٨	T	M	С
	Ħ	127	3	4	4	21
TRUE	٨	9	135	23	4	0
CLASS	Т	3	1	12	0	0
	134	0	5	n	123	1
	С	7	0	1	1	123

Probability of Correct Classification = .856

# CONFUSION MATRIX FOR THE TEST SET USING 33 FEATURES

LEGEND: H - HELICOPTER M - HUMAN A - APC C - C-131 T - HEAVY TRUCK

		ASSI	ASSIGNED CLASS			
		Н	٨	т	М	С
	Н	121	2	4	4	2
	Α	2	170	3	1	0
TRUE CLASS	Т	0	3	132	0	0
	М	0	1	0	133	2
	С	1	0	0	2	132

# CONFUSION MATRIX FOR THE DESIGN SET

# USING 22 FEATURES

		ASS	IGNED	CLA	SS	
		Н	٨	Т	Nf	С
	H	128	4	5	4	18
mp.un	٨	3	144	20	4	0
TRUE CLASS	Т	1	3	12	n	0
	1	0	5	0	123	1
	С	11	1	5	0	115

Probability of Correct Classification = .860

# CONFUSION MATRIX FOR THE TEST SET

# USING 22 FEATURES

LEGEND: H - HELICOPTER M - HUMAN  $\Lambda$  - APC C - C-131

T - HEAVY TRUCK

		ASSI	GNED	CLAS	<u>s</u>	
		H	٨	Т	М	С
	Н	120	2	4	4	3
TRUE	Α	3	170	2	1	0
CLASS	T	1	4	130	0	0
	М	2	1	0	129	4
	С	1	0	2	1	131

# CONFUSION MATRIX FOR THE DESIGN SET

# USING 16 FEATURES

		ASS 1	ASSIGNED CLASS			
		H	٨	Т	N	С
	H	129	2	5	4	19
TRUE	٨	6	142	19	4	0
CLASS	Т	1	3	12	0	0
	M	1	6	0	121	1
	С	11	1	6	0	114

Probability of Correct Classification = .853

# CONFUSION MATRIX FOR THE TEST SET

# USING 16 FEATURES

LEGEND: H - HEI ICOPTER M - HUMAN A - APC C - C-131 T - HEAVY TRUCK

Note that the probability of correct classification using the design set increases monotonically as the number of features is increased; while using the test set, it reaches its maximum value for 22 features and drops off.

Foley [2] points out a statistical trap involved with using the probability of error on the design as a measure of the true performance of the system when the ratio of the sample size to feature size is small. The probability of error or correct classification on the test set is the better measure and indicates that the probability of correct classification of 0.86 for the 22-feature design is the best performance.

The essential difference between the 22-feature design and the 16-feature design is that the former is based on measurements of both one and five second data segments, whereas, the latter is based solely on measurements of five second segments. Therefore, the exclusion of one second measurements not only reduces the dimensionality of the decision logic from 22 to 16, but it also simplifies feature extraction by elimination of the one second phase of the extraction process. The trade-off between the slightly superior performance of the 22-feature design (Pcc on the test set of 0.86) versus the simplicity and ease of implementation of the 16-feature design clearly

ranks the 16 feature design ahead of the 22-feature design.

The linear discriminants for the 16-feature logic design are given in Appendix C. These linear discriminants contain the ten weight vectors with their respective thresholds and, together, with the block diagram in Figure 13, completely define the pairwise Fisher logic for the 16-feature design.

#### SECTION X

#### DISCUSSION AND RECOMMENDATIONS

In many waveform classification problems, the classifier is designed entirely from features extracted from a waveform data base which is representative of each class. To insure that the data base is representative, data must be collected for a sufficient number of runs of each intrusion variation (speed, path, direction, etc.), so that the data for each variation is truly representative. Emphasis must be placed on the generality of a data base and not on its size alone. For example, to design a classifier which will detect most trucks, the data base must contain data from a wide variety of different type trucks, all operating at a number of sampled speeds and carrying loads which vary from maximum capacity to empty. The wider the variety of vehicles within a class, the more complex the data analysis becomes because all the variations and the possible combinations of the variations have to be sampled and analyzed for each variety of vehicles.

The mair goal of this effort is the development of a seismic classifier which will satisfy an acceptable error criteria regardless of where the classifier is located.

The seismometer response to an intrusion target is the signal which results from the convolution of the target signature

with the impulse response of the earth. The earth's impulse responses differ greatly throughout the world because they are determined by the geology and terrain of the locale. These impulse responses or transfer characteristics are not necessarily constant between two points in a locality but may change periodically as a function of the seasonal variations. Seasonal variations in the transfer characteristics are caused by changes in either the height of the water table, the depth of the frost line, or amount of snow cover. Therefore, it may not be realistic to believe that one seismic logic design might perform satisfactorily in any location or for an extended period of time in a locality which has extreme seasonal variations.

The key to the general seismic classifier design problem is the discovery of waveform features which contain adequate discriminatory information and are invariant to geographical location and seasonal variation. This report does not shed any light on the theory that such features exist, but it does exercise the procedures required to determine their existence. The importance of the data collection and data analysis procedures cannot be over emphasized. Before data analysis can yield meaningful results, the data base must contain data collected from selected test sites which are representative of the various types of terrain, geology, and seasonal variations found throughout the world.

# APPENDIX A

# BATCH PROGRAM LISTINGS

```
PROGRAM TO STRIP SPECIFIED DATA CHANNELS FROM A BAMK! TAPE
             AND WRITE A NEW TAPE WITH A SIMPLIFIED FORMAT.
C
      COMMON IDAT(320, 7), JCOUNT(45)
      COMMON /JAZZ/IA(1858) , IEOF, IBORT, IPARTY
      COMMON/JIM/LA(326)
      COMMON/AVERGE/IAVG(45), LCOUNT(45), IJK, NTIMES, IPRINT
      DIMENSION KCOUNT (45)
      IPARTY=0
      IBCRT = C
      IJKEU
      READ 1001, NUM, (KCOUNT (J) J=1, NUM)
 1001 FOR MAT (4012)
      READ 1003, NREC, NTIMES
 1003 FOFMAT(215)
      HEAD 1001, IPRINT
      DO 400 I=1.NUM
      INL=KCOUNT(I)
      WRITE(6,1006) I, IND
 1006 FORMAT(10X, THRECORD , 12, 17H IS FROM CHANNEL , 12)
  400 LCGUNT(IND)=1
      DO 3 J=1,45
  3
      JCCUNT(J)=0
      LO 1005 N=1, NREC
      CALL SPAWN(N.NUM, KCOUNT)
      IF(IEOF, EQ. 1) GO TO 1004
      IF(I60PT.NE.0) GO TO 1005
      IF(IJK, NF.0) GO TO 1005
      10 1000 Ja1, NUM
      LA(4)=1AVG(J)
LO 500 [=7,326
  500 LA(1)=1DAT(1-0,J)
      CALL PROC
 1000 CONTINUE
 1005 CONTINUE
 1004 IF(IJK.E2.0) GO TO 1007
      IF(IEOPT.NE.0) GO TO 1007
      UO 65 1=1.NUM
      IND=KCOUNT(I)
      KEND#UCOUNT (IND)
      00 66 J=KEND,320
66 [DAT(J, [)=0
      LA(4)=IAVG(1)
      LO 67 J=7,326
     LA(J)=1DAT(J-6,1)
 67
  65 CALL PROC
1907 CALL WEF
      CALL WEF
      CALL WEF
      STUP
      END
```

```
SUBROUTINE SPANN ( JPARM , NUM , K COUNT)
C
      CUMMON/JIM/LA(326)
      COMMON /JAZZ/IA(1858) , IEOF, IBORT, IPARTY
      COMMON IDAT(320, 7), JCOUNT(45)
      COMMON/AVERGE/IAVG(45), LCOUNT(45), IJK, MTIMES, IFRINT
      DIMENSION 100(4), JOD(32), JP(14)
      DIMENSION KCOUNT (45), MASK (3), KONST (3)
      DIMENSION FAVG(45)
      DATA [HALF/262144/
      EATA (JP(1), I=1,14)/1,21,1,12,22,30,1,12,1,12,31,39,40,45/
      DATA KM/0/77777770000/
      DATA(MASK(I), [=1,3)/0777700000000,000077770000,0000000007777/
      LATA (KONST(1), 1=1,3)/16777216,4096,1/
      DATA MASKA, MASKB/077777700000C, 0000600777777/
40
      FORMAT(8(2x, 112))
      CALL BELLED
      IF (IFOF. FQ. 1) RETURN
      IF (JEARM.NE.1) GO TO 2
      LA(3) = AND(IA(2), MASKA)/IHALF
      LAD4C=AND(IA(2), MASKR)
      ISAMF = MTIMES
      NTIMES=1000/ISAMP
      RECORD=0.
      100(1) = AND(14(1), MASKA)/ THALF
      IOD(2)=AND(IA(1),MASKB)
      ICU(3) = AND(IA(2), MASKA)/IHALF
      100(4) = AND (1A(2), MASKB)
      IF(LA04C.NF.100(4)) GO TO 7
       IF(LA(3).E0.100(3)) GO TO 5
       IF ( IF ORT )6, 19, 10
  5
      IF ( | HORT ) 6, 8, 5000
      CALL HSF
      CALL WEF
      IBORT=1
      GO TC 5000
      IF (LA(3).E0, IOD(3)) GO TO 11
      IF(IHOPT)6,19,10
      IF(I+ORT)6,12,10
  11
  19
      IF(IJK.EG.O) Go To 9
      10 65 1=1 NUM
       IND=KCOUNT(I)
      KEND=JCOUNT (IND)
      DO 66 J=KEND. 320
  56
      IDAT ( J. ! ) = 0
      LA(4)=IAVG(I)
      DO 67 J=7,326
      LA(J)= [ [AT(J-6, I)
      CALL PROC
      60 TO 9
      CALL BSF
  12
```

```
CALL WFF
10
    RECORD=0.
    IJK=U
B
    LA(1)=10D(1)
    LA(2)=ISAMP
    LA(3)=10D(3)
    LA04C=10D(4)
    LA(5) = AND(TA(228), MASKE)
    LA(6) = AND (1A(229), MASKA) / IHALF - 40
    IF(LA(6).GE,0) GO TO 3
    LA(5)=LA(5)-1
    LA(6)=1000+LA(6)
IF(IJK.GT.0) GO TO 444
    00 50 J=1, NUM
    IND=KCCUNT(J)
    JCOUNT([ND)=1
50
    IC= 2
    DO 1600 NN=1.8
    LO 800 MM=1,10
    DO 400 K=1,9,2
    JBE = JP (K)
    JPE=JP(K+1)
    MED
    IC=IC+1
    DO 400 J=JBE.JPE
    M=M+1
    1F(M,LT,4) GO TO 401
    IC=IC+1
    ME1
401 [F(JCOUNT(J).E0.0) GO TO 400
     I1=AND(IA(IC), MASK(M))
    I1=I1/KONST(M)
    IF(11.GE.2048) 11=0R(11.KM)
    J1=JCOUNT(J)
    L1=LCOUNT(J)
    IDAT(J1,1.1)=11
    JCOUNT(J)=JCOUNT(J)+1
400 CONTINUE
    IF(MM-2)600,700,800
600 JBE=JP(11)
    JPE=JP(12)
    GO TO 402
700 JBE=JP(13)
    JPE=JP(14)
402 M=0
    1C=1C+1
    DO 500 J=JRE.JPE
    M=M+1
    IF(M,LT,4) GO TO 501
    ICEIC+1
    M=1
```

```
501 [F(JCOUNT(J).EQ.0) GO TO 500
       I1=AND(IA(IC), MASK(M))
       II=I1/KONST(M)
       IF(I1,GE,2048) I1=OR(I1,KM)
       J1=JCOUNT(J)
       L1=LCOUNT(J)
       IDAT(J1,L1)=11
       JCOUNT(J)=JCOUNT(J)+1
  500 CONTINUE
800
      CONTINUE
       NNP=4+NN
       NN4=NNP-3
       DO 900 KZ=NN4, NNP, 2
       IC=IC+1
       KZP#KZ+1
       JOD(KZ) = AND(IA(IC), MASKA)/IHALF
900
       JOD(KZP)#AND(IA(IC), MASKB)
1000
      IC=IC+5
       IF (IPRINT.EQ.0) GO TO 64
       WRITE(6,45)(10D(1),1=1,4)
  45
      FORMAT(1H0,4(2X,010))
      WRITE(6,46)(JOD(1),1=1,32)
  46
      FORMAT(10X,012,2110,2X,012)
      IJK=IJK+1
      CO 5001 I=1.NUM
      IF (IJK. NE. NTIMES) GO TO 20
      IJKaC
      RECORD=RFCORD+1.
      DO 48 M=1, NUM
      FMEAN= 0.
      DO 60 J=1,320
      FDAY= IDAY(J, M)
      FMEAN = FDAT + FMEAN
      FMEAN=FMEAN/320.
      FAVG(M) = ((RECORD-1.) + FAVG(M) + FMEAN) / RECORD
      WRITE(6,47) FHEAN, FAVG(M)
  47
      FORMAT(10X,14HRECORD MEAN = .F12.4, 16H PARTIAL MEAN = .F12.4)
      IAVG(M) =FAVG(M)+0.5
  48
  20
      IF (IPARTY, NE.1) GC TO 5001
      IND*KCOUNT(I)
      WRITE(6,111) IND
  111 FORMAT (5X, AHCHANNEL , 12)
      KEND#JCOUNT(IND)-
      hRITE(6,40) (IDAT(J,1),J#1,KEND)
5001 CONTINUE
      IPARTY=0
5000
      RETURN
      END
```

		_1	2	LBL	SYMDEF	INE TO READ BAMKI TA BELLED
			3		SYMREF	BSF
	0000	10 .	4		BLOCK	JAZZ
	00000		5	JZ	BSS	1859
	00350		6	IBORT	BSS	1
	00350		7	IPARTY	_	1
	00001		8		USE	PREVIOUS
	00000	0 0	9	BELLAD		
00000		010				•
00000		010				
00000		010				
00000		010				
00000		000	10		LDA	=-2,DL
00000		010	11		STA	STR
00000		000	12		MME	GEINOS
00000		000	13		RTB	EG BOU
00001		011	14		ZERO	FC,DCW
00001		010	15		ZERO	STR
00001		ეცა <b>01</b> 0	16 17		MME LDA	GEROAD STR
00001		010	18		ANA	=0070000000000
00001		010	19		CMPA	±003000000000
00001		010	20		TZE	ABORT
00001		010	21		CMPA	<b>*</b> 0040000000000
00002		010	22		TZE	EOF
00002		000	23		LĎA	=0,DL
00002		010	24		TRA	RETURN
	NARY CARD SUBROUT!					== == =
00002		000	25	ABORT	LDA	=1,DL
00002		030	26		STA	IPARTY
00002		010	27		TRA	RETURN+1
00002		000		EOF	LDA	=1,DL
00002		030		RETURN		JZ+1858
00003		010	30		RETURN	BELLRD
00003		000		FC	BCI .	1,000001
00003	2 010000 003502 00003	030		DCW	BSS	J7,1858 2
	5000	, ,	0.5	314	003	•
ERROR	LINKAGE					
00003	5 000000000000	000				
00003		000				
LIT	ERALS					
00004	0 0700000000000	000				
06004		000	-			
00004		000				
	NARY CARD SUBROUT					
			34		END	

			00000	0	2		SYMDEF Block	PROC, WEF, BSF
			00000	0	4	JZ	BSS	326
			00000		5		USE	PREVIOUS
			00000	Ŏ	6	PROC	SAVE	0,1
1	000000	0000047		010	•			• •
	000001	0000002		000				
	000002	0000002		000				
	000003	0003336		010				
	000004	0003337		010				
	000005	0003337		010				
	000006	0000007		010				
	000007	0000017		010				
	000010		2200 03	000	7		LDXO	≖0,DU
	000011		2210 03	000		81G	LDX1	*0,DU
	000012	010000		030	9	LOOP	LDQ	JZ,0
	000012	000015		010	10	LOOF	TPL	G01
	000014	00001		000	11		SBQ	:1,DL
	000015	000024		000	15	G01	QLS	20
	000016	000022		000	13	301	LLS	18
							ADXO	
	000017	000001		000	14			±1,0U
	000020	010000		030	_15		ruo	J7.0
	000021	000023		010	16		TPL	G02
	000022		1760 07	000	17		SBQ	=1,DL
		RY CARD			4.0			
	000023	000024		000	18	G02	OLS	20
	000024	000022		000	19		LLS	18
	000025		7550 11	010	20		STA	IA,1
	000026	000001		000	21		ADXO	=1,DU
	000027	000001		000	22		ADX1	*1,DU
	000030	000243		000	23		CMPX1	=163,DU
	000031	000012		010	24		TNZ	LOOP
	000032	000001		000	25		MME	GEINOS
	000033	15 0000		000	26		WTB	
	000034	000064		011	27		ZERO	FC.DCW
	000035	000066		010	28		ZERO	STR
	000036	000002		000	29		MME	GEROAD
	000037	0000617		010	30		RETURN	PROC
			00004		31	WEF	SAVE	
	000040	0000427		010				
	000041	0003336		010				
	000042	0003337	54000	010				
	000043	0003337		010				
	000044	000001		000	32		MME	GEINOS
(	000045	55 0000	020001	000	33		WEF	
END (	OF BINA	RY CARD						
	000046	000064		010	34		ZERO	FC
	000047	000066		010	35		ZERO	STR
	000050	000002		000	36		MME	GEROAD
	000051	0000417		010	37		RETURN	WEF
			00005			BSF	SAVE	

20920	02	04-0	3-73	16,687					
	0000	152	000054	716000	010				
 	0000	153	000333	630790	910				
	0000	154	000333	754000	010				
	0000	155	J00333	741000	010				
	0000	156	000001	0010 00	000	39		MME	GFINOS
	0000	057	47 000	0 020001	000	40		BSF	
	0000	060	000064	000000	010	41		ZERO	FC
 	0000	061	000066	000000	010	42		ZERO	STR
	0000	062	J00UL 2	0(10 00	000	43		MME	GEROAD
	0000	-	000053	710000	010	44		RETURN	BSF
	0000	164	200000	000502	000	45	FC	RC1	1,000002
	0000	165	J00u70	000243	010	46	DCW	IOTO	14,163
		2		00006		_	STR	BSS	2
				00007	0	4 R	IA	BSS	163

# ERROR LINKAGE

000333 00000000000 000 000334 475146232020 000 END OF BINARY CAFD SUBPOUTI

END 336 IS THE NEXT AVAILABLE LOCATION.

GMAP VERSION/ASSEMBLY DATES JMPA 110171/102971

THERE WERE NO WARMING FLAGS IN THE ABOVE ASSEMBLY JMPB 110171/102971

					2		SYMDEF	( 9 TRACK VERSION ) PROC, WEF, BSF
			0000		3		BLOCK	JIM
			00000		4	JZ	BSS	326
			00000		5		USE	PREVIOUS
		20.00	00000		6	PRCC	SAVE	
	000000		710000	010				The second secon
	000001 000002		630000	010				
-	000003		754000	010				
	0000004	-	741000 2260 03	019	-			-0.54
	000005		2710 03	000	7	010	LDXO	=0,DU
	000006		2360 10	00 U 03 U	Ą	BIG	LDX1	≥0,DU
	000007		6(50 00	010	10	<b>LOOP</b>	LDQ TPL	72,0
	000010		1760 07	000	11		SPO	G01 =1,DL
	000011		7360 00	000	12	G01	OLS	20
	000012		7370 00	000	13	901	LLS	18
	000013		0600 03	000	14		ADXO	mi,DU
	000014		2360 10	030	15		LDO	JZ,0
	000015		6150 00	010	16		TPL	G02
	000016		1760 07	000	17		SBO	:1,DL
	000017		7360 00	000	18	GQ2	QLS	20
	000020		7379 0J	000	19		LLS	18
	000021	000163	7550 11	010	20		STA	IA,1
	000055	006061	0600 03	000	21		ADXO	<b>±1,</b> 0U
END	OF BINA	RY CAND	SUBPOUTI					
	000023	000001	0610 03	000	22		ADX1	<b>=1,</b> DU
	000024	000243	1(10 03	000	23		CMPX1	#163,DU
	000025	900006	6610 00	010	24		TNZ	LOOP
	000026	000011	0010 00	000	25		MME	GEINOS
	000027	15 010	<u> </u>	000	26		WTB	(Territoria)
	000030		066154	011	27		ZERO	FC, DCW
	000031		oruŭOŭ	01)	28		ZERO	STR
•	000032		0(10 00	000	29		MME	GERDAD
	000033		2350 00	01)	3 n		LDA	DCMA
	000034		7550 00	011	31		STA	DCW91
	000035		22 0 03	001	32		FUX0	=0,DU
	000036		2210 03	00)	3.3		LDX1	=0,DU
	000037		2360 10	031		L0069	LDO	J7.0
	000040		7360 00	00)	35		OLS	20
	000041		7370 00	009	36		LLS	16
	000042		2360 10	030	37 38		T10	J7+1,0
	000043		7360 00 7370 00	000	39		QLS	20 16
	000044		2360 10	030	40		LLS	
END			SUBROUTI	030	J			JZ+2,0
	000046		7360 00	000	41		QLS	20
	000047		7379 00	200	42			4
	000050		7550 11	010	43		LLS Sta	JA,1
	000051		7370 00	000	-			
	000052		2360 10	030	44		LLS LDQ	12
	000052		7360 00		45		QLS	JZ+3,0
	001.022	900924	1000 00	0 Ú J	40		<b>UL 3</b>	20

20920	02 04-	03-73	10,688					
	000054	000020	7370 00	000	47		LLS	16
	000055		2360 10	030	48		LPO	JZ+4.0
	000056		7360 00	000	49		QLS	20
	000057		7370 00	000	50		LLS	8
	000060		7550 11	010	51		STA	JA+1,1
	000061		7370 00	000	52		LLS	6
	000062		2360 10	030	53		r jig	JZ+5•1
	000063		7360 00	0 0 0	54		QLS	20
	000064		7370 00	000	55		LUS	16
	000065		2360 10	030	56		F 0.0	J7+6,0
	000066		7360 00	000	57		OLS	20
	000067		7377 80	000	58		LLS	12
	000070		7550 11	010	59		STA	JA+2,1
END			SUBPOLITI					4
	000071		7371 00	0011	6.0		LLS	4
	000072		2369 10	030	61		<u> </u>	JZ+7, n
	000073	-	7360 00	000	62		QLS	20
	000074		7371 00	000	6.3		LLS	16
Mary statement appropriate and an	000075		2361 10	030	64		r)a	JZ+8,0
	000076 000077		7360 00 7370 00	000 000	65		JLS JLS	20 16
	000100		7550 11	010	67		STA	JA+3,1
	000101		0600 03	000	68		ADXO	<b>±9,</b> nU
	000102		1000 03	000	69		CMPXJ	=324, DU
	000103		6600 00	010	70		TZE	QUIPUT
	000104		0610 03	000	71		ADXT	=4, pu
	000105		7100 00	010	72		TRA	LOUPS
	000106		0110 00	000	73	OUTPUT	MME	GEINOS
	000107		0.0000	000	74		WTB	
	000110	000153		011	75		ZERO	FC9.DCW91
	000111	006161	000000	010	76		ZERO	STR9
	000112	000002	0110 00	000	77		MME	GEROAD
	000113	000001	<b>0</b> 619 00	000	7 A		MME	GEINOS
END	OF BINA	CARD YR	SUBROUTI					
	000114		, U20001	000	79		WFF	
	000115	000152		010	80		ZFRO	FC
	000116	000157		010	81		ZERO	STR
	000117		0619 00	000	82		MME	GERDAD
	000120	0000017		016	83		RETURN	PROC
	202121	0064043	00012	_	84	WEF	SAVE	
	000121	0001237		010				
	000122			010				
	000123	0006467		018 010				
	000124		0610 00	000	85		MME	GEINOS
-	000125		(2)001	000	86		WEF	6.1000
	000127	000153		010	87		ZERO	FC9
Appear, in expense of	000127	000161		010	88		ZFRO	STR9
	000131		0610 00	000	89		MME	GEROAD
	000132	0001227		010	90		RETURN	WEF
			00013			BSF	SAVE	
	000133	0001357	10000	010	-			

	000134	00064663LU		014			100 1	
	000135	1006467540	5 <b>0</b>	010				
	000136	6006467410	00	010				
EN	ID OF BINAL	HY CARD SUB	ROUTT					
	000137	000011 001	0 60	000	35		MME	GEINOS
	000140	47 0600 62	0001	000	93		BSF	
	000141	000152 000	-	010	94		ZERO	FC
	000142	000157 000	000	010	95		ZERO	STR
	000143	000005 001	0 00	000	96		MME	GFROAD
	000144	000001 001	U UJ	000	97		MME	GF INOS
	000145	47 0000 02	0001	000	48		BSF	
	000146	000153 000	100	010	49		ZERO	FC9
	000147	000161 000		010	100		ZFRO	STR9
	000150	000002 001	0 00	000	101		MMF	GERCAD
	000151	0001347100	0.0	910	102		RETURN	BSF
	000152	00000000000	02	2011	163	FC	BCI	1,0000002
	000153	00000000000	0.3	000	164	FC9	801	1,000003
	000154	100163 000	243	UIN	105	DCW	1010	IA,163
	000155	000426 000	220	210	106	DCW9	loid	JA,144
			000156		107	DCM91	855	1
			000157		108	STR	<sub>ยร</sub> ร	2
			000161		109	STRS	885	2
			000163		110	T.A.	655	163
			000426		111	JA	ess	144
			00470		TTI	JA	C . 3	\$13.4

### ERROR LINKAGE

000646 000000000000 000 000647 475146232020 000 END OF BINARY CARD SUBROUTI

650 IS THE NEXT AVAILABLE LOCATION.

GMAP VERSION/ASSEMBLY LATES JMPA 110171/102971

THERE WERE NO WARLING FLAGS IN THE ABOVE ASSEMBLY

#### NINE TRACK MAGNETIC TAPE VERSION

```
SEISMIC SENSOR DATA FEATURE EXTRACTOR
C
C
             NINE TRACK MAGNETIC TAPE VERSION
      ALBERT H. PROCTOR
                              12 SEPTEMBER 1972
C
                                                       HUNEYWELL 635 FORTRAN IV
      NCHAN IS THE MAXIMUM NUMBER OF DATA CHANNELS TO BE PROCESSED
¢
      FROM ONE RUN OR THE NUMBER OF MAG TAPE PASSES.
C
      WRUNS IS THE NUMBER OF RUNS TO BE PROCESSED IN THE NEXT PASS.
C
C
      ITRESH IS THE THRESHOLD VALUE FOR THE ABSOLUTE AVERAGE DEVIATION
      FROM THE MEAN FOR EACH 1.024 SECOND WINDOW.
IRUN IS AN ARRAY CONTAINING THE RUN NUMBERS TO BE PROCESSED IN
C
C
Ç
      THE NEXT PASS.
Ç
      TCHAN IS AN ARRAY CONTAINING THE CHANNEL NUMBERS TO BE PROCESSED
      FOR EACH RUN IN THE NEXT PASS.
C
      DIMENSION JHEAD(6), IBUF(6144), JTAIL(6), ITEMP(6), ICHAN(20), IRUN(20)
      DIMENSION X(6144), FEAT(100)
      EQUIVALENCE (X, IBUF), (JHEAD(7), IBUF(1))
      IFC=1
      READ (5, 1001) NCHAN
      DO 21 KCHAN=1, NCHAN
      READ(5, 1000) NRUNS, ITRESH
1000
      FORMAT(215)
      READ(5, 1001)
                       (IRUN(I), Im 1, NRUNS)
      FORMAT (4002)
1001
      READ(5,1003) (ICHAN(I), I=1, NRUNS)
      PORMAT(4012)
1003
      WRITE(6, 1004) NRUNS, ITRESH
 1004 FORMAT(1H0, 1X, 7HRUNS = , I3, 3X, 8HITRESH =, I5)
      WRITE(6, 1008) (IRUN(I), I=1, NRUN5)
 1008 FORMAT(1HO.1X,4HRUNS,5X,16(2X,02))
      WRITE(6, 1012) (ICHAN(I), I=1, NRUNS)
 1012 FORMAT (2x, 8 HCHANNELS, 1x, 16 (2x, 12))
      CALL REW
      DO 20 I=1, NRUNS
      NVECT=0
      CALL RD9(JHEAD(1), ICHAN(I), 0,0, IFC, IEOF)
       IF (IEOF, NE, O) GO TO 1
       IF(JHEAD(3), EQ, IRUN(I)) GO TO 2
       CALL PSF
       GO TO 1
       ISTART=321
2
       JSTART=1
       ISHIPT=0
       DO 40 J=ISTART,5120,320
      IF(0,50.1) GO TO 31
       DO 30 II=1,6
      JII=J+II-7
      ITEMP(II)=IBUF(JII)
  30
      CALL RD9(IBUF(J-6), ICHAN(I), 0, 0, IFC, IEOF)
      IF(IEOF.NE.O) GO TO 20
      IF(J.EQ.1) GO TO 40
      DO 4 II=1,6
```

#### NINE TRACK MAGNETIC TAPE VERSION

```
JII#J*II=7
      JTAIL(II) = IBUF(JII)
      IBUF(JII) = ITEMP(II)
 40 CONTINUE
      DO 6 J=JSTART,5120,1024
      1=3+1023
      MEAN=JTAIL(4)
      ISUN=0
      DO 5 R=J.L
      ISUM=ISUM+IABS(IBUF(K)-MEAN)
      ISUM=ISUM/1024
      PRINT 2001, ISUM
2001 FORMAT (10X, 2015)
      IF(ISUM.GE.ITRESH) GO TO 6
      TSHIFT=L
      CONTINUE
      JTAIL(5)=JTAIL(5)=4
      JTAIL(6)=JTAIL(6)=800
      IF(JTAIL(6).GE.O) GO TO 84
      JTAIL(6) = 1000+JTAIL(6)
      JTAIL(5)=JTAIL(5)=1
 81 PRINT 1005, JTAIL, ICHAN(I)
 1005 PORMAT(1x,012,2x,15,2x,012,2x,4(15,2x))
      IF(ISMIFT.EQ.0) GO TO 8
      33=1
      JSTART=1
      IF(ISHIFT.GE.5120) GO TO 70
      IDIF=5420-ISHIFT
      JSTART=IDIP/1024
      JSTART=JSTART+1024+1
      ISHIFT=IDIF/320
      ISHIFT=5121-(ISHIFT*320)
      DO 7 J=ISHIFT,5120
      IBUF(3J)=IBUF(J)
      33=33+4
      ISTART-JJ
70
      GO TO 3
      DO 100 J=1.5120
  100 X(J)=IBUF(J)
     1.4
      SUM 1=0.
      SUM2=0.
      DO 10 J=1,1024,512
      CALL REGAR(X(J),X(5121),R)
      SUN 1=8UM 1+R
  10 SUM2=SUM2+R+R
      PEAT(%)=SUN1/2.
     1=1+1
      PERT(L)=SUM2/2.
      L=L+1
```

#### NINE TRACK MAGNETIC TAPE VERSION

```
BQ 11 J=1025,5120,512
      CALL REGAR(X(J),X(5121),R)
      SUM 1=BUM 1+R
      SUM2=FUM2+R*R
      PEAT(L)=SUH1/10.
      L=L+
      PEAT(1) = SUM2/10.
      LPL-1
      1151
      DO 200 J=1,3
      M=2=(3/3)
      CALL DOUBLE (X(L1), X(L2), M)
      19-11-2048
      12=12+2048
200
      DO 9 J=513, 1024
      x(J)=[x(J-512)+x(J)+x(J+1536)+x(J+2048)+x(J+3984))/5.
      CALL HARMON(X,6,40,4,FEAT(L),FEAT(L+1))
      L=1+2
      CALL BINRAT (X, 2, FEAT(L), FEAT(L+1))
      L=1+2
      CALL THRESH(X, 2, 4, FEAT(L))
      1=1+4
      CALL SPECVT(x, 12, 101, PEAT(L), PEAT(L+12))
      L#1+13
      CALL PEKPIK(X.2.0.1.FBAT(L))
      171-1
      CALL HARMON(X(513),6,40,4,FEAT(L),FEAT(L+1))
      L=L+2
      CALL BINRAT(X(513),2,FEAT(L),FEAT(L+1))
      1=1+2
      CALL THRESH (X(513),2,4,FEAT(L))
      1=1-4
      CALL SPECYT(X(513), 12, 101, PEAT(L), PEAT(L+12))
      1-1+13
      CALL PERPIK(X(513),2,0.1,PEAT(L))
      PRINT 2000, (PEAT(IND), IND=1, L)
 2000 PORMAT(10X, 10210,3)
      PUNCH 1005. JTAIL. ICHAN(I)
      M=1
      DO 12 J=1,1,6
      2487+5
      TP(L1.GT.L) L1=L
      PUNCH 2002, (FEAT (IND), IND=J, L1), M
 2002 PORMAT (6E12,4,18)
  12 M##+1
      NYECT-NYECT+1
      ISTART-1
      JETART=1
      GO TO 3
```

# 01 04-04-73 17,796 SEISHIC SENSOR DATA FEATURE EXTRACTOR NINE TRACK HAGNETIC TAPE VERSION

20 PRINT 2003, NVECT
2003 FORNAT(20H TOTAL VECTORS = ,I5)
21 CALL REW
STOP
END

23842 WORDS OF MEMORY USED BY THIS COMPILATION

The second of th

```
SUBROUTINE DOUBLE(X,Y,NUM)
            THIS SUBROUTINE ENABLES THE CALCULATION OF THE
             POWER SPECTRUMS OF TWO REAL WAVEFORM SEGMENTS
      C
            WITH ONE CALL TO THE FFT SUBBOUTINE.
            DIMENSION X(1024),Y(1024),S1(1024),S2(1024),TAB(780)
           IF(NUM=1) 30,25,30
           DO 27 J=1, 1024
      25
           Y(J)=0.
      27
      30
            CALL PFT(10,-1.0,X,Y,S1,S2,TAB)
            IF(NUM-1) 285,400,285
      285
            DO 300 K=2,512
            1-1026-K
            A=X(K)+X(L)
            B=X(K)-X(L)
            C=Y(KT+Y(L)
           D=X(K)=Y(L)
           X(R)=(A+A+D+D)+.25
      300
           Y(K)=(C+C+B+B)+.25
           X(1)=0.
           x(513)=0.
           DO 320 K=2,512
           M=K+512
      320
           X(M)=Y(K)
           RETURN
      400
           DO 450 K=2,512
            AWI(K)*X(K)
            B=Y(K)+Y(K)
      450
           X(K)=A+B
           x(1)=0.
           RETURN
            END
><><><\
```

DOES NOT APPEAR IN READ, DATA, COMMON OR LEFT OF EQUALS (=) 

DOES NOT APPEAR IN READ, DATA, COMMON OR LEFT OF EQUALS (=) 52 >>>>>>>>>>>>>>>>>>>

TAB DOES NOT APPEAR IN READ, DATA, COMMON OR LEFT OF EQUALS (=) 

23721 WORDS OF MEMORY USED BY THIS COMPILATION

```
SUBROUTINE FFT(NSTAGE, SIGN, XR, XI, SCRAT1, SCRAT2, SCRAT3)
      ALBERT H. PROCTOR 21 JANUARY 1972 HONEYWELL 635 FORTRAN IV
      NSTAGE IS THE LOG BASE 2 OF N WHERE N IS THE NUMBER OF DATA POINTS
C
      TO BE PROCESSED
С
     SIGN IS THE TRANSFORM/INVERSE TRANSFORM PLAG.
      SIGN IS -1. FOR THE TRANSFORM AND 1. FOR THE INVERSE TRANSFORM.
      XR WILL CONTAIN THE REAL PART OF EITHER THE INPUT OR OUTPUT DATA.
C
      XI WILL CONTAIN THE IMAGINARY PART OF FITHER THE INPUT OR OUTPUT DATA.
C
      SCRAT1 AND SCRAT2 ARE SCRATCH ARRAYS OF LENGTH N.
      SCRAT3 CONTAINS THE COSINE TABLE OF LENGTH 3/4 N.
C
      DIMENSION XR(2), XI(2), SCRAT1(2), SCRAT2(2), SCRAT3(2)
      DATA LSTAGE/0/
      IF (SIGE) 12, 11, 11
  11 ASSIGN 6 TO ISIGN
      GO TO 13
    ASSIGN 7 TO ISIGN
  12
  13
     IF (NSTAGE-LSTAGE) 14, 5, 14
 14
      LSTAGE=NSTAGE
      N=2**NSTAGE
      N2=N/2
      FLTN=N
      PHI2N=6.2831853/FLTN
      NPI=N2+1
      NPI1=NPI+1
      ガイニカノサ
      NFT2=N4+1
      N3FI2=3+N4+1
      SCRAT3(1)=1.
      SCRAT3(NPIZ)=C.
      SCRAT3(NPI)=-1.
      SCRAT3(N3PI2)=0.
     Do 1 I=2,N4
      FI=I-1
      TEMP=FI*PHI2N
      TEMP=COS (TEMP)
      SCRAT3(I)=TEMP
      ISUB=N2+I
      ISUB1=vpI1-I
      SCFAT3(ISUB) =-TEMP
      SCPAT3(ISUB1) == TEMP
      L= 1
      DO 3 J=1.NSTAGE
      NI=I
      L=2*L
      N2J=N/L
      NP=N2J
      DO 2 I=1,NI
      IN2J=(I-1)*N2J
      IN2K=IN2J+1
      IN2JI=IN2K+N4
      W1=SCRAT3(IN2K)
```

```
01 04-03-73 18,926
            GO TO JSIGN, (6.7)
            W2=-SCRAT3(IN2JI)
        6
            GO TO 8
            W2= SCRAT3(IN2JI)
            DO 2 IR=1, NR
            ISUB=IR+IN2J
            ISUB 1=ISUB+IN2J
            ISUB2=ISUB1+N2J
            ISUB3=ISUP+N2
            WR=W1*XR(ISUB2)-W2*XI(ISUB2)
            WI=W2*XR(ISUB2)+W1*XI(ISUB2)
            SCRAT1(ISUB)=XR(ISUB1)+WR
            SCRAT2(ISUB)=XI(ISUB1)+WI
            SCRAT1(ISUB3)=XR(ISUB3)-WR
            SCRAT2(ISUB3)=XI(ISUB1)-WI
        2
            CONTINUE
            DO 3 IR=1, N
            XR(IR)=SCRAT1(IR)
            XI(IR)=SCRAT2(IR)
        3
            IF(SIGN) 10.9.9
            DO 4 IR=1, N
            XR(IR) = XR(IR)/FLTN
            XI(IR)=XI(IR)/FLTN
            RETURN
            END
```

23647 WORDS OF MEMORY USED BY THIS COMPILATION

```
SUBROUTINE HARMON (PS, NPEAKS, ISTART, MARGIN, SPACE, COUNT)
        THIS SUBROUTINE DETERMINES THE MOST FREQUENTLY OCCURRING
C
        PAIRWISE SPACING BETWEEN THE LARGEST PEAKS IN THE POWER
C
      SPECTRUM AND THE NUMBER OF TIMES IT OCCURRED, DIMENSION PS(512), KCOUNT(20), ITAB(20), IFRE2(10)
č
      DO 9 I=1.NPEAKS
      LPEAK=ISTART
      PEAK=PS(ISTART)
      JSTART=ISTART+1
      DO 1 J=JSTART, 512
IF(PEAK, GE, PS(J)) GO TO 1
      LPEAK=J
      PEAK=PS(J)
      CONTINUE
      IF(PEAK.LT.O.) GO TO 17
      IFREQ(I)=LPEAK
      PS(LPEAK) =-PEAK
      JSTART=LPEAK+1
      DO 4 J=JSTART,512
      PSJ=PS(J)
      IF(PSJ.LT.0.) 30 TO 5
      DIF=ABS(PS(J-1))-PSJ
      IF(DIF.GE.O.) GO TO 4
      TEST=50.*(PEAK-ABS(PS(J-1)))
      IF(TEST.GT.PEAK) GO TO 5
      PS(4)=-PSJ
      JJJ=J+1
      DO 3 JJ=JJJ,512
      PSJ=PS(JJ)
      IF(PSJ.LT.0.) 40 TO 5
      DIF=ABS(PS(JJ=1))=PSJ
      IF(DIF)3,33,33
  3
      PS(JJ)=-PSJ
      GO TO 5
      PS(J)==PSJ
      GO TO 5
      JSTART=JJ+1
      PS(J)=-PSJ
      GO TO 2
      JSTART=LPEAK-1
      DO 8 JJ=1, JSTART
      J=JSTART=JJ+1
      PSJ=PS(J)
      IF(PSJ.LT.O.) GO TO 9
      DIP=PSJ-ABS(PS(J+1))
      IF(DIF.LE.O.) GO TO 8
      TEST=50.*(PEAK-ABS(PS(J+1)))
      IF(TEST.GT.PEAK) GO TO 9
      PS(J)=-PSJ
      JJJ=J-1
      DO 7 JJJJ=1,JJJ
```

```
01 04-03-73 18,937
            3=333-3333+1
            PS.J=PS(J)
            IF(PSJ.LT.O.) GO TO 9
            DIF=PSJ-ABS(PS(J+1))
            IF(DIF)77,77,7
            PS(J)=-PSJ
            GO TO 9
            PS(J)=-PSJ
            GO TO 9
           JSTART=J-1
            PS(J)=-PSJ
            GO TO 6
        9
            CONTINUE
            GO TO 18
        17
            NPEAKS=I-1
           DO 10 I=1,512
        18
            PS(I)=ABS(PS(I))
            CALL SORTUP (IFREQ, NPEAKS)
            K=0
            DO 11 I=1,20
        11 KCOUNT(I)=0
            N1=NPEAKS-1
            DO -15 I=1,N1
            JSTART=I+1
            DO 15 JEJSTART, NPEAKS
            IDIF=IfREQ(J)-IfREQ(I)
            MIN=IDIF-MARGIN
            MAX=IDIF+MARGIN
            IF(K.EQ.0) GO TO 13
            DO 12 KK=1,K
            IF (ITAB(KK), LE, MAX, AND, ITAB(KK), GE, MIN) GO TO 14
            CONTINUE
            IF(K.GE.20) GO TO 15
            K=K+1
        13
            ITAB(K)=IDIF
            KK=K
        14
            KCOUNT(KK)=KCOUNT(KK)+1
        15
            CONTINUE
            IND#1
            MAXMUM=KCOUNT(1)
            DO 16 I=2,K
            IF (MAXHUM.GE.KCOUNT(I)) GO TO 16
            IND=I
            MAXMUM=KCOUNT(I)
        16 CONTINUE
            COUNT=KCOUNT(IND)
            SPACE=ITAB(IND)
            RETURN
```

END

```
SUBROUTINE SORTUP (IRAY, M)
        THIS SUBROUTINE IS CALLED BY HARHON TO ORDER THE M LARGEST PEAKS ACCORDING TO THEIR AMPLITUDES,
C
       DIMENSION IRAY(N)
       # 1=#-1
       DO 2 X=1,81
       INDOI
       LITTLE=IRAY(I)
       JSTART=I+1
DO 1 JmJSTART, N
       IP(IRAY(J), GE, LITTLE) GO TO 1
       LITTLE=IRAY(J)
       INDOJ
       CONTINUE
       ITEMPOIRAY(I)
       IRAY(I)=LITTLE
       IRAY (IND) -ITEMP
       RETURN
       END
```

23709 WORDS OF MEMORY USED BY THIS COMPILATION

		CHOROLITANE T. DEC. /DC . CYART LEVEL C B.CTA
		SUBROUTINE THRESH (PS, ISTART, LEVELS, PIST)
	C	THIS SUBROUTINE COMPARES THE AMPLITUDES OF
	C	ELEMENTS IN THE POWER SPECTRUM AGAINST A NUMBER
	000	OF EQUALLY SPACED THRESHOLDS AND RETURNS THE
	C	NUMBER OF ELEMENTS WHICH FALL BETWEEN THESE
	C	THRESHOLDS,
		DIMENSION PS(512), PIST(LEVELS)
		PEAK*PS(ISTART)
		SMALL=PEAK
		JSTART=ISTART+1
	•	DO 1 J=JSTART, 512
		SMALL = AMIN1 (SMALL, PS(J))
	1	PEAK=AMAX1(PEAK,PS(J))
		DIVIDE=(PEAK-SMALL)/FLOAT(LEVELS)
		DO 3 Je1, LEVELS
	3	PIST(J)=0,
	-	DO 4 1=1START, 512
		IND=(Ps(I)-sMALL)/DIVIDE+1.
		IF(IND, GY, LEVELS) IND#LEVELS
	4	PIST(IND)=PIST(IND)+1.
	·	RETURN
		END
23780	WARNS	OF MEMORY USED BY THIS COMPILATION
20/00	# U \ U J	or action, comp p. title com tention

23648	WORDS	OF MEMORY USED BY THIS COMPILATION
		RETURN END
	4.0	SUM=SUM+SCRAT(L) R=(512.+XMAS)/SUM
		SUM=0. DO 40 L=1,512 XMAS=AMAX1(XMAS,SCRAT(L))
		SCRAT(!)=ARS(X(!)-SUM) XMAS=0.
	20	SUM=SUM/512, DO 20 1=1,512
	10	SUM=0. DO 10 I=1,512 SUM=SUM+X(I)
	С	GIVEN 1/2 SECOND WINDOW OF THE TIME WAVEFORM, DIMENSION X(512), SCRAT(512)
	Č	MEAN TO THE AVERAGE DEVIATION FROM THE MEAN IN A
	C C	THIS SUBROUTINE CALCULATES R, WHERE R IS DEFINED AS THE RATIO OF THE MAXIMUM DEVIATION FROM THE
		SUBROUTINE REGAR(X, SCRAT, R)

-		SUBROUTINE BINRAT (PS. ISTART, FEAT1, FEAT2)
•	С	THIS SUBROUTINE CALCULATES THE RATIOS OF ENERGY
i	Ċ	BETWEEN ONE AND THENTY HERTZ AND BETWEEN FORTY-ONE
	Č	AND SIXTY HERTZ TO THE ENERGY BETWEEN TWENTY-ONE
,	Ċ	AND FORTY HERTZ.
,	•	DIMENSION PS(512)
,		SUM1=0.
j		SUMŽ=0.
)		SUM3=0,
)		ISTOP=ISTART+19
		DO 1 I=ISTART, ISTOP
!		SUM1=SUM1+PS(I)
5		SUM2=SUM2+PS([+20)
ŀ	1	SUM3=SUM3+PS(I+40)
;		FEAT1=SUM1/SUM2
)		FEAT2=SUM3/SUM2
,		RETURN
}		END

23648 WORDS OF MEMORY USED BY THIS COMPILATION

	С	SUBROUTINE SPECVY(PS, NVECT, ITH, VECT, REATEB) THIS SUBROUTINE CALCULATES THE RATIO OF ENERGY
	Č	ABOVE A SPECIFIED FREQUENCY TO THE ENERGY BELOW
	-	AND ALSO CREATES A VECTOR WHOSE COMPONENTS
	C	CONTAIN NORMALIZED ENERGY VALUES FRON CONSECUTIVE
	C	FREQUENCY BINS OF THE POWER SPECTRUM. DIMENSION PS(512), VECT(NVECT)
		DO 1 I=1.NVECT
	1	VECT(1)=0.
		SUM=0.
		DO 5 I=1.NVECT
		J=5+1-3
		K=5+[+1
		DO 2 L=J,K
	2	VECT(I)=VECT(I)+PS(L)
	5	SUM=SUM+VECT(I)
		DO 6 I=1, NVECT
	6	VECT(1)=VECT(1)/SUM
		RGYaT=0,
		RGYAT=0,
		DO 3 I=1, ITH
	3	RGYBT=RGYBT+PS([)
		J=11H+1
		DQ 4 I=J,512
	. 4	RGYAT=RGYAT+PS(I)
		REATEB=RGYAT/RGYBT .
- to		RETURN
		END

C C	SUBROUTINE PERPIK(PS,ISTART,THRESH,COUNT) THIS SUBROUTINE CALCULATES THE NUMBER OF PEAKS IN A POWER SPECTRUM WHICH ARE ABOVE SOME SPECIFIED
Ċ	PERCENTAGE OF THE MAXIMUM PEAK.
C	DIMENSION PS(512)
	XMIN=PS(ISTART)
	AMAS=XMIN
	INIT=ISTART+1
	DO 1 1 = INIT, 512
	XMIN=AMIN1(XMIN,PS(I))
1	XMAS=AMAX1(XMAS,PS(I))
•	TEST=(XMAS-XMIN)+THRESH
	COUNT=0.
	PSMIN=PS(I)-XMIN
	IF(PSMIN.GT.TEST) GO TO 2
	ISWIT=0
	GO TO 3
2	ISWIT=1
3	00 5 1=2,512
	PSMIN=PS(I)-XMIN
	IF (ISWIT, E0, 1) GO TO 4
	IF (PSMIN.GT.TEST) ISWIT=1
	GO TO 5
4	IF (PSMIN, GT, TEST) GO TO 5
	1SW17±0
	COUNT=COUNT+1,
5	CONTINUE
	RETURN
	END
	C'75

# 1 LBL FSF, REW, SUBBOUTINE TO SKIP RECORDS AND REWEND HAG TAPES 2 AL PROCTOR, ISCP, RADC

			3	SINDER	TSP, RIW
		000000	4 FSF	SAYE	
	000000	000002710000 01			
	000001	000033630000 01	)		
	000002	000033754000 01	)		
	000003	000033741900 01			
	000004	000001 0010 00 00	5	MME	GEINOS
	000005	45 0000 020001 00		757	
	000006	000039 909000 010	7	ZERO	TC
	000007	000034 000000 010	6 7 8 9	ZERO	STATUS
	000010	000002 0010 00 00	9	MMB	GEROAL
	000011	000031 2350 00 010		LDA	STATUS
	000012	000011 0050 00 010		TPL	LOOP1
	000013	000001710000 010		RETURN	PST
		000014	13 REW	SAYE	
	000014	000016710000 010			
	000015	000033630000 040			
	000016	000033754000 010			
	000017	000033741000 040			
	000020	000001 0010 00 000		MME	GEINOS
	000021	70 0000 020001 000		REW	
	000022	J00030 000000 010		ZERO	rc
END		RY CARD FSF00002		•	
	000023	000031 000000 010	17	ZERO	STATUS
	000024	000002 0010 00 000		MME	GEROAL
	000025	000031 2330 00 010		LDA	STATUS
	000026	000025 5050 00 010		TPL	LOOP2
	000027	000015710000 010		RETURN	REW
	000030	000000000001 000		BCI	1,000001
		000031	23 STATUS		2

#### ERROR LINXAGE

000033 00000000000 000 000034 266225202020 000 END OF BINARY CARD FSF00003

24 END
36 IS THE NEXT AVAILABLE LOCATION.

GHAP VERSION/ASSEMBLY DATES JMPA 110171/102971 JMPB 110171/102971
THERE WERE NO WARNING PLAGS IN THE ABOVE ASSEMBLY

	1 *	LBL R:	EAD9TRI	K, SUBR , RADC	OUTIN	E TO	READ 9 TR	ACK DECODED TAPES	
					3		SYNDEP	RD9	
			00000	0	4		USE	PREVIOUS	
			00000	0	5	RD9	SAVE	0,1,2,3,4,5	
	000000	003010710	000	010				And the same at the property of the state of	
	000001	000000220		000					
	000002	000000221	003	000					
	000003	000000222		000					
	000004	000000223	003	000					
	000005	000000224		000					
	000006	000000225		000					
	000007	003045630		010					
	000010	003045754		010					
	000011	003045741		010					
	000012	000001740		01)					
	000013	000002741		010				orara a . will	
	000014	000003742		01)					
	000015	000004743		010					
	000016	000005744		010					
	000017	000006745		010				2.4	
	000020	000002 23		000	6		LDA	2.1	
	000021	003044 75		010	. 7	-	STA	BUF	
T. W. D.	000022	000007 45		000	9		STZ	7.1*	
END	000023	RY CARD RE			•			£ 4+	
	000023	000006 23		000	10		LDA STA	.6,1* FC	
	000024	000000 22		010 000	11		LDXO	=0,DU	
	000025	003041 23		010	12		LDA	DUMMY	
	000027	000134 73		010	13		STX	TALLY	
	000030	003040 23		010	14		LDA	DUMMYB	
-	000031	000133 75		010	15		STA	TALLYB	
	000032	000001 20		00)	16		MYE	GEINOS	
	000033	03 0000 7		000	17		RT9		
	000034	003043 00		011	18		ZERO	FC.DCW	
	000035	000136 07		01)	79		ZERO	STR	
	000036	000002 00		00)	20		MME	GEROAD	
	000037	000136 23		012	21		LDA	STR	
	000040	000002 73		000	22		ALS	2	
	000041	777400 37	50 03	000	23		AVA	=0777400,DU	
	000042	211400 11	50 03	000	24		CMPA	=0211400,00 9 TRACK E	OF
	000043	000047 60	דס סס	017	25	-	TNZ	TOOP	
	000044	000001 23	50 07	000	26		LDA	=1,DL	
	000045	000007 75	50 31	202	27		STA	7.1*	
END	OF BINA	RY CAPD RE	AD9TRX						
	000046	000132 71		017	28		TRA	EXIT	
	000047	003050 23		010		LOOP	LDQ	=1472	
	000050			002	30		<b>QL5</b>	-6	
	000051	000134 75		013	31		STCQ	TALLY, 06	
_	000052	003050 23		010	32		LDQ	=1472	
	000053	000006 73		000	33		QLS	6	
	000034	000133 75	20 06	013	34		STCQ	TALLYB, 06	

20915	02 04-	03-73	13.957					e man and a sun garagement of
	000055	00.133	2350 52	010	35	RUN	LDA	TALLYB, SC
	000056	000134	7550 52	010	36		STA	TALLY, SC
	000057	000055	6070 00	01)	37		TTF	RUN
	000060	000001	0500 03	000	38		ADXO	=1,DU
	000061	000004	1000 03	000	39		CMPXO	=4,DU .
	000062	000047	6010 00	010	40		TNZ	LOOP
	000063		2240 03	00)	41		LDX4	=0,DU
	000064		2230 03	007	42		LDX3	≖0,DU
	000065		2360 31	00)	43	START	LDQ	3,1*
	000066	000124	6000 00	010	44		TZE	NEXI
	000067		1760 00	01)	45		<b>SBQ</b>	<b>-1</b>
	000070	003052	4020 00	(1)	46		MPY	=109
END	OF BINA	RY CARD	READSTRK					
	000071		6230 06	000	47		EAX3	0.QL
	000072	000000	2200 03	00)	48		LDXO	■O, DU
	000073	000140	2360 13	01)	49	BEGIN	LDQ	IA,3
	000074	003053	2350 00	01)	50		LDA	<b>=</b> 0
	000075	000022	7370 00	007	51		LLS	19
	000076	003044	755C 70	01)	52		STA	BUF. *O
-	000077	000001	0500 03	00)	53		ADXO	=1,DU
	000100		7370 00	000	54		LLS	13
	000101		7350 00	00)	55		ALS	18
	000102		7310 30	00)	56		ARS	24
	000103	003044	7550 70	01)	57		STA	BUF, * )
	000104		0630 03	000	58		ADX3	=1,DU
	000105		0600 03	000	59		ADXO	=1,DU
	000106	000000	2220 03	000	60	LOOPX	LDX2	=0,DU
	000107	003053	2350 00	<b>010</b>	61		LDA	=0
	000110	000140	2360 13	010	62		LDQ	IA,3
	000111	000014	7370 00	000	63	LOOPY	LLS	12
	000112	000030	7350 00	00)	64		ALS	24
	000113	000030	7310 00	202	65		ARS	24
END	OF BINA	RY CARD	READSTRK					
	000114	003044	7550 70	313	66		STA	BUF, *O
	000115	000001	0600 03	000	67		ADXO	=1,DU
	000116	000001	0620 03	000	68		ADXZ	=1,00
	000117	000003	1020 03	000	69		CMPX2	=3,DU
	000120	000111	6010 00	01)	70		TNZ	LOOPY
	000121	000001	0630 03	000	71		ADX3	=1,DU
	000122	000506	1000 03	000	72		CMPXO	=326, DU
	000123	000106	6010 00	010	73		TNZ	LOOPX
	000124	000001	0610 03	000	74	NEXT	ADX 1	=1,00
	000125	000506	2250 03	000	75		LOX5	=326, DU
	000126	003044		010	76		ASX5	BUF
	000127	000001	0640 03	000	77		ADX4	=1,DU
	000130	000003	1040 03	00)	78		CMPX4	=3,DU
	000131		6016 00	010	79		TYZ	START
	000132	0000017		010	80	EXIT	RETURN	R69
			00013	_	81	TALLYB	BSS	1
			00013		82	TALLY	BSS	1
	000135	000140		010	83	DCW	IOID	IA,1472
			00013	_		STR	355	2

0915	02	04-(	3.	-7	3		17		54	8											
<b>PW</b> N		040 BINAI	-		14	•		0	Ö	01 40 TR	•		0			IA DUMMYB	BSS		1472 IX, 1	472,0	
END		041						0	0	00	-		0			DUMMY	TAL	LY	IX, 1	472.0	
		in aggregation on the same				-	-			30 30						FC	BSS	•	1		
E	RRO	R LI	K	A G	E																
		045										00							2. 2	5 W	
	003	046	5	12	41	12	02	0 :	20			00	0			,					
sandra-regionospedes	1	ITER	L	5																	
		050 051			000							00									
	-	052 053			000							00							<del></del>		
END	07	BINAL	Y	C	AR	D	RE	AI	9	TR	K				91		END		-		
		THE												ON	•	171/102			- M D R	110171/	10297
		RE														ABOVE			01120		
																			-		
						_	<del></del>	_	_												

```
SEISMIC SEVER FEATURE TAPE GENERATOR
C
        THIS IS THE COS 1604 PROGRAM WHICH CONVERTS DATA CARDS TO
C
C
        AN OLPARS COMPATIBLE MAGNETIC TAPE.
       PROGRAM ALSDATA
        DIMENSION X(130), 1X(130), NUM(20), INAME(20), LFOR(20), IHEAD(7)
       EQUIVALENCE (X, IX)
       READ 1007, 15KIP
 1 07 FORMAT(15)
       READ 1000, LFOR
       READ 1000, I VAME
 1.00 FORMAT(10A8)
       READ 1001, NDIM, ITOT, NUM
       NP3=NDIM+3 & VLD=NDIM+1
 1.01 FORMAT(2513)
       DO 7 1=1.1541P
       READ TAPE 10
       DO 1 IDUM#1, ITOT
ITOP=NUM(IDJM)
       DO 2 1=1,173P
       READ 1006, HEAD
 1.06 FORMAT(1X,112,2X,15,2X,012,2X,4(15,2X))
       READ LFOR, (X(J), J=1, NDIM)
 1002 FORMAT(15(1X,F3.0))
[X(ND]M+1)=[HEAD(1)+100000+[HEAD(3)+16000+[HEAD(7)+1000+[HEAD(5)
       IX (ND1M+2)=INAME(IDUM).AND.778
       IX (NDIM+3) = INAME (IDUM)
       WRITE TAPE 10, (X(JJ), JJ=1, NP3)
    2 CONTINUE
    1 CONTINUE
       PAUSE
       END FILE 10
       REWIND 10
 PRINT 1005
1:05 FORMAT(1H1)
    6 READ TAPE 10, (X(KK), KK=1, NP3)
       IF (EOF, 10)4,5
 5 PRINT 1003, (X(KK), KK=1, NDBM)
1 03 FORMAT(1X, 10E11, 3)
       PRINT 1004. (X(KY), KK=NLO, NP3)
 1 04 FORMAT(1X+110+2(1X+AB)+//)
       GO TO 6
    4 REWIND 10
       END
```

#### APPENDIX B

### PROBABILITY OF CONFUSION MEASURES

## PAIR C/H RANKINSS

RANKING	MEASUREMENT	CONFUSION
1	27	.2165970482
į	5	3068226121
3	46	3732664996
Ă	29	.3880813144
5	24	
-		.3964912281
6	35	4010025063
7	7	.4328599276
8	43	.4407128933
9	21	4484544695
10	13	.4613756614
11	3	.4906711222
12	42	15032024506
13	14	.5131161236
14	44	5141186299
14 15	39	.5157894737

## PAIR C/A RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	47	1407407407
2	25	1407407407 177777778
3	46	1975589225
4	6	3091750842
5	35	3121212121
6	13	.3153619529
7	24	3385942761
Á	27	
ě		.3649831650
	28	.3835437710
10	42	.3838383838
11	14	.3832154882
12	36	.3911616162
13	5	.4061868687
14	39	4077861953
15	29	4292929293

## PAIR M/A RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	4	.0561497326
2	3	.0635026738
3	46	,2376336898
4	1	.2516711230
5	45	.2650401069
6	2	.3091577540
7	24	.3629679144
8	23	.3723262032
9	31	.3983957219
10	32	.4044117647
11	43	4124331551
12	44	.4278074866
13	22	4776069518
14	26	4799465241
15	39	.4986631016

## PAIR M/T RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	43	.0294662309
2	38	.0368191721
3	44	0589324619
4	45	.0813180828
5	16	.0958605664
6	42	.0960784314
7	37	1326797386
8	22	1547930283
9	21	1552287582
10	29	.1839869281
11	20	.1844226579
12	39	.2139978213
13	23	.2141612200
14	15	.2213507625
15	7	.2430827887

# PAIR T/A RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	37	.0528619529
2	29	·1239898990
3	15	1548400673
4	38	1654882155
5	16	.2099326599
6	7	.2109427609
. 7	36	.2450336700
8	42	13030723906
.9	14	.3070286195
10	35	.3277356902
11	45	.373989899n
12	20	.3907407407
13	13	.4133838384
14	41	4287878788
15	19	.4436 <sub>0</sub> 26936

#### PAIR M/H RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	3	1114551084
Ž	4	1116209642
3	28	1258292791
4	43	1416961521
7	27	•156 <sub>0</sub> 7 <sub>0</sub> 3229
6	6	11620964175
7	21	1868089341
8	5	2001879699
9	31	.2449690402
10	32	2453007519
11	41	·2606700575
12	19	.2757076515
13	44	12904135338
14	1	.3104820876
14 15	2	3405572755

# PAIR C/T RANKINGS

•	RANKING	MEASUREMENT	CONFUSION
	1	38	.0518518519
	2 3	16	.0962962963
	3	39	·1037 <sub>0</sub> 37 <sub>0</sub> 37
	4	17	.2296296296
	5	46	•237 <sub>0</sub> 37 <sub>0</sub> 37 <sub>0</sub>
	5	37	.244444444
	~ <b>7</b>	47	.2518518518
	8	25	.266666667
	9	45	+2740740741
	10	44	2740740741
	11	24	.355555556
	12	15	.3629629630
	13	23	.3851851852
	14	43	• 4000000000
	15	22	.422222222

## PAIR C/M RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	42	.1402505447
2	43	.2583877996
3	6	.2655773420
4	29	.2873638344
5	28	2956427015
6	20	.3023965142
7	31	.3097494553
8	4	3177559913
ŏ	32	•31791939 <sub>00</sub>
4.0	3	
10		.3248910675
11	47	.3321895425
12	26	.346732 <sub>0</sub> 26 <sub>1</sub>
13	27	.3769607843
14	21	.3907952070
15	25	.3983660131

# PAIR A/H RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	5	.1431989064
ž	27	.1660970608
3	28	.2137303486
4	6	.2252648667
5	41	.3320232399
6	19	.3413790157
7	40	,4427973342
8	18	.4636876282
9	43	.4642002734
10	21	4959415584
11	47	.5 <sub>0</sub> 37593985
12	17	.5260167464
13	42	.5320403281
14	3	.5331937799
15	20	.5337064251

## PAIR T/H RANKINGS

RANKING	MEASUREMENT	CONFUSION
1	16	.1048175996
ž	38	1195210248
3		1272626009
3	29	
4	7	.1490392648
5	37	.1493734336
6	27	.2309663046
7	15	.2608187134
8	5	2683375104
9	17	.3206349206
10	39	3874129769
ii	45	4200501253
12	4 ö	.4253411306
13	18	4409356725
14	3	4774157616
15	42	.4802005012

### APPENDIX C

## LINEAR DISCRIMINANTS

```
FISHER LOGIC
     **************
                                    NODES IN SET
                             APC A BIG T MEN M 131 C
                     HEL H
  PAIR 1
                           + NODE APC A - NODE HEL H
                                                                     FISHER
                                     COEFICIENTS
3.96813970E-02 = 9.68449165E-04 -4.89501481E-03 5.46598674F-02 = 2.72921703E-01 6.97331329E-03 = 8.28998958E-03 6.64553796E-02 2.90634536F-01 -4.76369896E-02 -4.58998220E-02 6.04166410E-01 7.42977735E-02 -4.74997161F-01 -4.54152691E-01
-1.58537605E-01
                                     THRESHOLDS
-3.90074135E 00
                  PAIR 2
                           + NODE BIG T - NODE HEL H
                                                                     FISHER
                                     COEFICIENTS
4.69708409E-02 -1.93562543E-03 1.48660333E-04 6.44628818F-03 -4.76223767E-02 1.23024713E-01 -4.76777325E-03 3.53239344E-01 2.90515473F-01 5.56283819E-02 1.04713262E-02 -4.16778187E-01 -5.20485980E-01 -4.10062826F-01 -3.99207157E-01 -2.79211913E-02
                                     THRESHOLDS
-2.17537000E 00
                           + NODE BIG T - NODE APC A
                                                                    FISHER
         PAIR 3
                                    COEFICIENTS
4.60801584E-02
                                     THRESHOLDS
```

-4.34867354E-01

```
PAIR 4
                                        + NODE HEN M
                                                                  - NODE HEL H
                                                                                                   FISHER
                                                      COEFICIENTS
2.31412790E-02 -8.29361174E-04 -4.87289242E-04 1.56959376F-02 2.45615090E-01 -7.35585459E-02 -2.31964098E-03 -5.11421164E-01 -5.83638325F-01 -2.47784696E-02
-6.03075430E-02 4.75379822E-01 2.85305202E-01 5.51895298F-02 1.28423779E-01
-1.06921944E-02
                                                      THRESHOLDS
 -9.64285189E-01
              PAIR 5
                                                                  - NODE APC A
                                        + NOBE MEN M
                                                                                                   FISHER
                                                      COEFICIENTS
6.38509513E-02 -2.92688890E-03 -1.22036734E-04 1.63364582F-03 7.74779748E-02 -8.68381015E-02 -1.97395633E-05 -3.60530052E-01 -3.92612416F-01 -4.50913730E-02
-8.48406086E-02 3.15413584E-01 1.80348321E-01 4.55969276F-01 5.89007129E-01
  4.708087428-02
                                                      THRESHOLDS
  2.35755267E-01
              PAIR
                                        + NODE MEN M
                                                                  - NODE BIG T
                                                                                                   FISHER
                                                     COEFICIENTS
                          5.73910040E-03 1.72406718E-04 1.92032559F-03 3.13769992E-02 4.48998653E-04 -1.85814095E-01 -1.76911342F-01 -2.15106346E-02 4.46816622E-01 4.81252016E-01 5.63346962F-01 3.96430146E-01
-5.50894445E-02
-1.18786829E=01
9.75774688E-02
  1.57187128E-02
                                                      THRESHOLDS
  1.42390262E-01
              PAIR 7
                                                               - NODE HEL H
                                                                                                   FISHER
                                        + NOBE 131 C
                                                     COEFICIENTS
9.81440973E-02 -4.44773076E-03 1.46881055E-04 -9.54345732F-04 2.58345800E-01 -2.16534455E-03 -9.81695737E-04 -2.62143802E-01 -7.81897234F-01 -1.10873436E-01 -2.93516114E-01 2.31881216E-01 1.00293123E-01 -1.48426786F-02 2.84237662E-01
  1.52502180E-02
                                                     THRESHOLDS
```

-1.45736931E-01

```
+ NODE 131 C - NODE APC A
                                                                                                                FISHER
                PAIR 8
 COEFICIENTS

3.68751710E-02 -1.93352649E-03 1.11484727E-04 -5.66834421F-03 5.10667510E-02

2.60469141E-04 1.73549076E-04 8.67489587E-01 -4.34033285F-01 -5.31094909E-02

-1.56387985E-01 4.40291408E-02 4.92898694E-02 7.95402735F-02 1.30704837E-01
  4,13119158E-03
                                                             THRESHOLDS
  1.77654615E-01
                                                                                                                FISHER
                PAIR 9
                                             + NODE 131 C - NODE BIG T
                                                            COEFICIENTS
-3.29124399E-02 3.38280485E-03 2.10909619E-04 -5.81299678F-03 4.30942207E-02 -6.16253086E-04 3.21567445E-04 -6.88160741E-01 -6.40371320F-01 -2.87653123E-01 -1.14154548E-01 7.20820436E-02 2.92250744E-02 6.36615539F-02 8.64491945E-02
 -1.14154548E-01
4.63701435E-03
                                                             THRESHOLDS
 -6.68589073E-02
                                             + NODE 131 C - NODE MEN M
                PAIR 10
                                                                                                                FISHER
                                                             COEFICIENTS
-1.45109285E-02 1.15913285E-03 4.11714251E-05 -1.46447234F-02 3.46032284E-02 2.98563366E-04 7.61958367E-04 1.11012423E-01 -7.58692477F-01 -2.96591145E-01 -5.60288311E-01 -6.88661871E-02 -5.03450867E-02 -3.53279527E-02 4.21597498E-03
  2.27725816E-03
                                                            THRESHOLDS
  1.83859536E-01
```

END OF THIS LOGIC SET

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